

PROGETTO ESECUTIVO

LAVORI DI ADEGUAMENTO STATICO E FUNZIONALE DEL PLESSO SCOLASTICO "SILVIO PELLICO"

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FASCICOLO DEI CALCOLI ANTE OPERAM

ELABORATO

R.3

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FASCICOLO DEI CALCOLI STATO DI FATTO

DIMOSTRAZIONE NUMERICA DELLA SICUREZZA DELL'OPERA E DEL RAGGIUNGIMENTO DELLE PRESTAZIONI ATTESE

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Il Progettista

MODELLAZIONE

La struttura è costituita da diversi elementi distinti, in base alla loro funzione, in

[lista elementi del modello]

I livelli di sicurezza scelti dal Committente e dal Progettista in funzione del tipo e dell'uso della struttura, nonché in funzione delle conseguenze del danno, con riguardo a persone, beni, e possibile turbativa sociale, compreso il costo delle opere necessarie per la riduzione del rischio di danno o di collasso, hanno indirizzato al progetto di una struttura con i seguenti requisiti:

- sicurezza nei confronti degli Stati Limite Ultimi (SLU)
- sicurezza nei confronti degli Stati Limite di Esercizio (SLE)
- sicurezza nei confronti di deformazioni permanenti inaccettabili: Stato Limite di Danno (SLD).

La struttura è stata schematizzata con un modello spaziale agli elementi finiti che tengono conto dell'effettivo stato deformativo e di sollecitazione, secondo l'effettiva realizzazione. I vincoli esterni della struttura sono stati caratterizzati, a seconda degli elementi in fondazione se presenti, con: travi winkler, plinti diretti, plinti su pali, platee; ovvero con vincoli perfetti di incastro, appoggio, carrello, ecc. I vincoli interni sono stati schematizzati secondo le sollecitazioni mutuamente scambiate tra gli elementi strutturali, inserendo, ove opportuno, il rilascio di alcune caratteristiche della sollecitazione per schematizzare il comportamento di vincoli interni non iperstatici (cerniere, carrelli, ecc.). Il modello agli elementi finiti è stato calcolato tenendo conto dell'interazione tra strutture in fondazione e strutture in elevazione, consentendo un'accurata distribuzione delle azioni statiche e sismiche; il calcolo viene eseguito considerando il comportamento elastico lineare della struttura. I solai sono schematizzati come aree di carico, sulle quali vengono definiti i carichi permanenti (QP Solai), carichi fissi (QFissi Solai) e variabili (QV solai); tali carichi vengono assegnati alle aste in modo automatico in relazione all'influenza delle diverse aree di carico. Le masse corrispondenti ai carichi

variabili sui solai nelle combinazioni sismiche vengono trattate in maniera automatica mediante un coefficiente moltiplicativo definito insieme alla tipologia del solaio.

Il modello utilizzato è stato valutato alla luce dei diversi scenari di carico a cui viene sottoposta la struttura durante la sua costruzione e la sua vita, atto a garantire la sicurezza e la durabilità della stessa. Per la tipologia strutturale affrontata non è stato necessario definire scenari di contingenza, quindi non è stata schematizzata la struttura durante le fasi costruttive, e si ritiene che non ci siano variazioni del modello di calcolo e degli schemi di vincolo, durante la vita dell'opera. Per il dettaglio degli scenari di calcolo si faccia riferimento alla "Relazione di Calcolo"

Il progetto e la verifica degli elementi strutturali è stato effettuato seguendo la teoria degli Stati limite. I parametri relativi alle verifiche effettuate sono riportati nella Relazione di Calcolo.

Il solutore agli elementi finiti impiegato nell'analisi è SpaceSolver, per il calcolo di strutture piane e spaziali schematizzabili da un insieme di elementi finiti tipo

- BEAM,
- PLATE-SHELL,
- WINK,
- BOUNDARY,

interagenti tra loro attraverso i nodi, con la possibilità di tenere in conto tutti i possibili disassamenti, mediante l'introduzione di concetti rigidi e traslazioni degli elementi bidimensionali. Il solutore lavora in campo elastico lineare, si basa sulle routines di Matlab ed è stato sviluppato in collaborazione con l'Università di Roma – Tor Vergata. Il solutore offre la possibilità di risolvere anche travi su suolo alla Winkler con molle spalmate sull'intera suola, anziché sul solo asse, plinti diretti e su pali, pali singoli, platee, piastre sottili e spesse con controllo delle rotazioni attorno all'asse normale alla piastra (drilling). Inoltre, per gli elementi BEAM considera il centro di taglio e non il baricentro.

L'affidabilità del solutore è stata testata su una serie di esempi campioni calcolati con altri procedimenti o con formule note, di cui si rende disponibile la documentazione.

AFFIDABILITA' DEI CODICI UTILIZZATI

Il programma è dotato di una serie di filtri di auto diagnostica che segnalano i seguenti eventi:

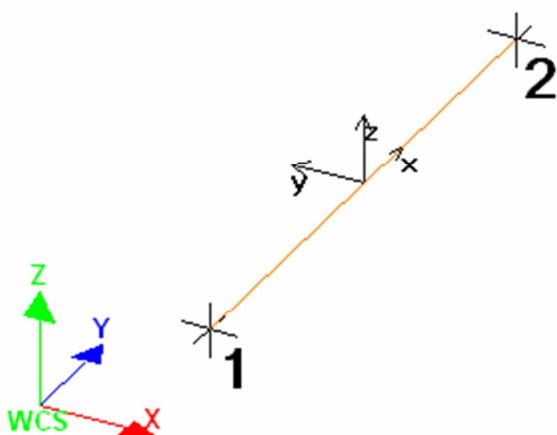
- labilità della struttura
- assenza di masse
- nodi collegati ad aste nulle
- mancanza di terreno sugli elementi in fondazione
- controllo sull'assegnazione dei nodi all'impalcato
- correttezza degli spettri di progetto
- fattori di partecipazione modali
- assegnazione dei criteri di verifica agli elementi
- numerazione degli elementi strutturali
- congruenza delle connessioni tra elementi shell
- congruenza delle aree di carico
- definizione delle caratteristiche d'inerzia delle sezioni

- presenza del magrone sotto la travi tipo wink
- elementi non verificati per semi progetto allo SLU, con inserimento automatico delle armature secondo i criteri di verifica.
- elementi non verificati allo SLU per armature già inserite nell'elemento strutturale
- elementi non verificati allo SLE per armature già inserite nell'elemento strutturale

PRESENTAZIONE DEI RISULTATI

I disegni dello schema statico adottato sono riportati nel fascicolo allegato alla presente relazione

E' stato impiegato il Sistema Internazionale per le unità di misura, con riferimento al daN per le forze.



Il sistema di riferimento globale rispetto al quale è stata riferita l'intera struttura è una terna di assi cartesiani sinistrorsa OXYZ (X,Y, e Z sono disposti e orientati rispettivamente secondo il pollice, l'indice ed il medio della mano destra, una volta posizionati questi ultimi a 90° tra loro).

La terna di riferimento locale per un'asta è pure una terna sinistrorsa O'xyz che ha l'asse x orientato dal nodo iniziale I dell'asta verso il nodo finale J e gli assi y e z diretti secondo gli assi geometrici della sezione con l'asse y orizzontale e orientato in modo da portarsi a coincidere con l'asse x a mezzo di una rotazione oraria di 90° e l'asse z di conseguenza.

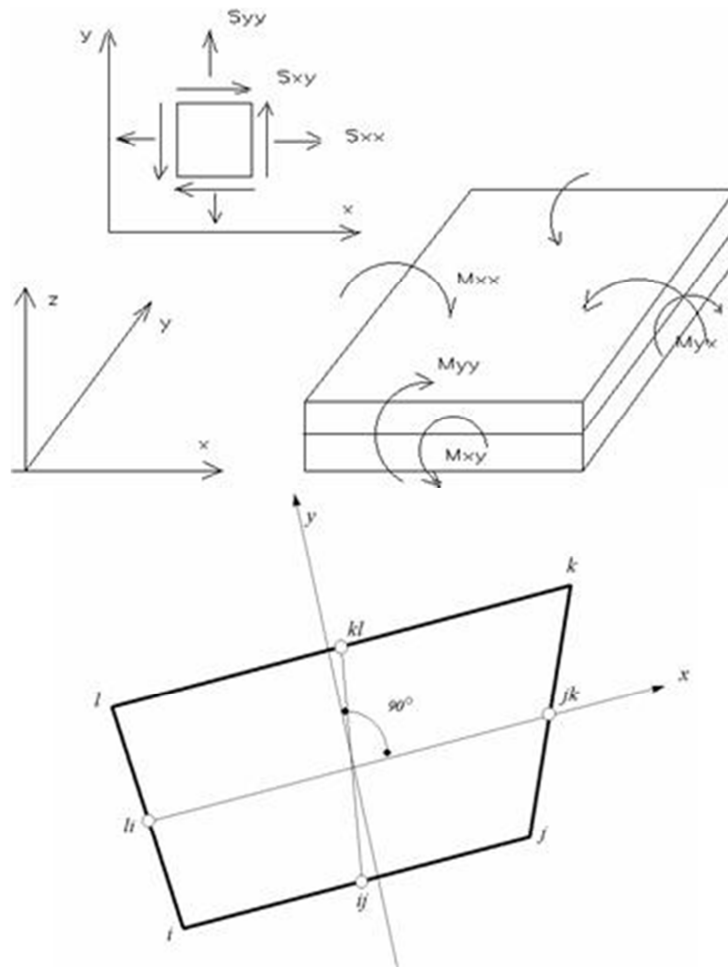
Per un'asta comunque disposta nello spazio la sua terna locale è orientata in modo tale da portarsi a coincidere con la terna globale a mezzo di rotazioni orarie degli assi locali inferiori a 180°.

- ? Le forze, sia sulle aste che sulle pareti o lastre, sono positive se opposte agli assi locali;
- ? Le forze nodali sono positive se opposte agli assi globali;
- ? Le coppie sono positive se sinistrorse.

Le caratteristiche di sollecitazione sono positive se sulla faccia di normale positiva sono rappresentate da vettori equiversi agli assi di riferimento locali; in particolare il vettore momento positivo rappresenta una coppia che ruota come le dita della mano destra che si chiudono quando il pollice è equi verso all'asse locale.

- ? Le traslazioni sono positive se concorde con gli assi globali;
- ? Le rotazioni sono positive se sinistrorse.

Il sistema di riferimento locale per gli elementi bidimensionali è quello riportato in figura



La terna locale per l'elemento shell è costituita dall'asse x locale che va dal nodo li al nodo jk, l'asse y è diretto secondo il piano dell'elemento e orientato verso il nodo l e l'asse z di conseguenza in modo da formare la solita terna sinistrorsa. L'asse z locale rappresenta la normale positiva all'elemento.

Le sollecitazioni dell'elemento sono:

a) sforzi membranali.

$$S_{xx} = s_x$$

$$S_{yy} = s_y$$

$$S_{xy} = t_{xy}$$

b) sforzi flessionali:

M_{xx} momento flettente che genera s_x , cioè intorno ad y.

M_{yy} momento flettente che genera s_y , cioè intorno ad x

M_{xy} momento torcente che genera t_{xy} .

Le sollecitazioni principali dell'elemento sono:

$$M_{1,2} = \frac{M_{xx} + M_{yy}}{2} \pm \sqrt{\left(\frac{M_{xx} - M_{yy}}{2}\right)^2 + M_{xy}^2}$$

$$S_{1,2} = \frac{S_{xx} + S_{yy}}{2} \pm \sqrt{\left(\frac{S_{xx} - S_{yy}}{2}\right)^2 + S_{xy}^2}$$

$$\tan 2\theta = \frac{M_{xy}}{M_{xx} - M_{yy}}$$

dove θ è l'angolo formato dagli assi principali di M1 e M2 con quelli di riferimento e

$$\tan 2\psi = \frac{S_{xy}}{S_{xx} - S_{yy}}$$

dove ψ è l'angolo formato dagli assi principali di S1 e S2 con quelli di riferimento

L'elemento shell usato come piastra dà i momenti flettenti e non i tagli in direzione ortogonale all'elemento che possono ottenersi come derivazione dei momenti flettenti;

$$T_{zx} = M_{xx,x} + M_{xy,y}$$

$$T_{zy} = M_{xy,y} + M_{yy,y}$$

quando invece viene usato come lastra ci restituisce una 's' costante ed una 't' costante non adatti a rappresentare momenti flettenti, ma solo sforzi normali e tagli nel piano della lastra.

I tabulati di calcolo contengono due sezioni principali: la descrizione del modello di calcolo e la presentazione dei risultati.

La descrizione del modello di calcolo contiene:

- ? i dati generali (dimensioni)
- ? le coordinate nodali;
- ? i vincoli dei nodi e i vincoli interni delle aste, con le eventuali sconnessioni;
- ? le caratteristiche sezionali;
- ? le caratteristiche dei solai;
- ? le caratteristiche delle aste;
- ? i carichi sulle aste, sui nodi e sui muri (inclusa la distribuzione delle distorsioni impresse, e delle variazioni e dei gradienti di temperatura);
- ? configurazione di sistemi che introducono stati coattivi;
- ? le caratteristiche dei materiali;
- ? legami costitutivi e criteri di verifica;
- ? le condizioni di carico;

La stampa dei risultati contiene:

- ? le combinazioni dei carichi;
- ? le forze sismiche agenti sulla struttura;
- ? gli spostamenti d'impalcato, se l'impalcato è rigido;
- ? gli spostamenti nodali;
- ? le sollecitazioni sulle membrature per ogni combinazione di carico;
- ? la sollecitazione sul terreno sotto travi di fondazione o platee;
- ? deformate;
- ? diagrammi sollecitazioni;

TABULATI DI VERIFICA

L'esito di ogni elaborazione viene sintetizzato nei disegni e schemi grafici allegati, che evidenziano i valori numerici nei punti e/o nelle sezioni significative, ai fini della valutazione del comportamento complessivo della struttura, e quelli necessari ai fini delle verifiche di misura della sicurezza.

Di seguito si riportano le tabelle relative a:

- Baricentri rigidezze e masse
- Fattori di partecipazione e masse modali

Centri di rigidezza e Centri di massa

Scenario di calcolo : **Set_NT_SLV_SLD_A2_(STR/GEO)**

Centri rigidezze

Piano	Kx	Ky	Kxy	K ϕ	X	Y	r/l>0.8
	kg/cm	kg/cm	kg/cm	kg*cm/rad	cm	cm	
1	5.181633E05	8.813430E05	2.768224E04	7.226437E11	1340	1517	0.950
2	1.690611E05	2.136950E05	8.281041E03	2.068671E11	1341	1504	1.033
3	1.280606E05	1.505814E05	5.882513E03	1.493562E11	1340	1515	1.045
4	9.280504E04	1.005896E05	3.453896E03	9.142804E10	1350	1548	1.857

Ellissi delle rigidezze

Piano	K ξ	K η	alfa	r ξ	r η
	kg/cm	kg/cm	°	cm	cm
1	5.160655E05	8.834409E05	-4	904	1183
2	1.675742E05	2.151819E05	-10	980	1111
3	1.266167E05	1.520253E05	-14	991	1086
4	9.149355E04	1.019011E05	-21	947	1000

Baricentri masse per posizione masse

Piano	Pos.Masse	X	Y	Peso Sism.
		cm	cm	kg
0	1	0	0	0
1	1	1379	1675	526683
2	1	1430	1699	82365
3	1	1369	1621	152333
4	1	1422	1672	88054

Periodi di vibrazione e Masse modali

Scenario di calcolo : **Set_NT_SLV_SLD_A2_(STR/GEO)_2018**

Posizione masse 1

Numero di Frequenze calcolate =15, filtrate=10

N	T(s)	Coeff. Partecipazione	Masse Modali	Percentuali
			kgm*g	

N	T(s)	Coeff. Partecipazione		Masse Modali		Percentuali	
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.3863	240.890	-60.685	569062	36115	66.99	4.25
2(2)	0.3385	-68.555	-245.907	46089	593012	5.43	69.81
3(3)	0.3000	79.147	-29.858	61431	8743	7.23	1.03
4(5)	0.1465	126.693	-6.225	157408	380	18.53	0.04
5(10)	0.1096	-26.766	-49.319	7026	23853	0.83	2.81
6(11)	0.1038	-2.917	85.836	83	72253	0.01	8.51
7(12)	0.1032	-10.876	23.689	1160	5503	0.14	0.65
8(13)	0.1004	1.016	41.075	10	16546	0.00	1.95
9(14)	0.0984	17.005	-18.607	2836	3395	0.33	0.40
10(15)	0.0936	2.740	-49.153	74	23693	0.01	2.79
Somma delle Masse Modali [kgm*g]				845178	783493		
Masse strutturali libere [kgm*g]				849435	849435		
Percentuale				99.50	92.24	99.50	92.24

Masse e coefficienti di partecipazione rotazionali:

N	T(s)	Coeff. Partecipazione	Masse Modali	Percentuali
			kgm*g	
1	0.3863	-1054.337	10901322	13.36
2	0.3385	-271.802	724478	0.89
3	0.3000	2318.805	52728963	64.61
4	0.1777	6.705	441	0.00
5	0.1465	-276.569	750115	0.92
6	0.1295	-77.394	58741	0.07
7	0.1200	193.501	367187	0.45
8	0.1169	758.112	5636220	6.91
9	0.1150	429.823	1811753	2.22
10	0.1096	-865.896	7352793	9.01
11	0.1038	-188.227	347444	0.43
12	0.1032	-74.228	54032	0.07
13	0.1004	-53.831	28418	0.03
14	0.0984	87.009	74242	0.09
15	0.0936	-58.347	33386	0.04

VERIFICHE STATO LIMITE ULTIMO

Verifica dei Pilastri

Scenario di calcolo : Set_NT_SLV_SLD_A2_(STR/GEO)_2018

Pilastro : 1 [1, 101]

Sez. R: By= 50.0 cm Bz=30.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificata**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00	

$v_{max}=N/(fcd*A)=0.169 \leq 0.65$ [Comb. (3+4)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-1-3(+)	-27384	-2060	-19842	10693	15968	10693	15968	0.50

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Sezione non verificata : Sezione non verificata									
Testa	(3+4)-I-3(+)	-26259	208	12323	10569	15859	10569	15859	1.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	14170	--	21145	23111	21145	6.70	2.500	1.5
Z	(3+4)-II-1	--	--	3236	15402	--	--	15402	6.70	2.500	4.8

Pilastro : 1 [101 , 201]

Sez. R: By= 50.0 cm Bz=30.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$v_{max}=N/(fcd*A)=0.054 \leq 0.65$ [Comb. (3+4)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	2(-)	-12314	-4098	-10158	9004	14286	9004	14286	1.2
Testa	(3+4)-I-3(+)	-7980	1754	4276	8504	13723	8504	13723	2.9

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	6324	--	18463	34667	18463	10.05	2.500	2.9
Z	(3+4)-II-1	--	--	3958	--	17776	19915	17776	10.05	2.500	4.5

Pilastro : 1 [201 , 301]

Sez. R: By= 50.0 cm Bz=30.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$v_{max}=N/(fcd*A)=0.049 \leq 0.65$ [Comb. (3+4)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(+)	-7970	1988	5283	8503	13721	8503	13721	2.3
Testa	(3+4)-I-3(+)	-7557	3871	9625	8454	13666	8454	13666	1.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	5978	--	18313	34667	18313	10.05	2.500	3.1
Z	(3+4)-II-1	--	--	3649	--	17631	19915	17631	10.05	2.500	4.8

Pilastro : 2 [2 , 102]

Sez. R: By= 50.0 cm Bz=30.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Non verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00	Sezione non verificata

$v_{max}=N/(fcd*A)=0.168 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-17963	-567	28571	9646	14976	9646	14976	0.38
Sezione non verificata : Sezione non verificata									

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Testa	(3+4)-I-1(+)	-16838	-276	-17791	9519	14843	9519	14843	0.75
Sezione non verificata : Sezione non verificata									

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	19570	--	19771	23111	19771	6.70	2.500	1.0
Z	(3+4)-II-2	--	--	1057	15402	--	--	15402	6.70	2.500	15

Pilastro : 2 [102 , 202]

Sez. R: By= 50.0 cm Bz=30.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$v_{max}=N/(fcd*A)=0.056 \leq 0.65$ [Comb. (3+4)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-8583	-774	12825	8574	13803	8574	13803	1.1
Testa	(3+4)-II-1(+)	-9014	3714	409	8624	13860	8624	13860	2.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	7037	--	18403	34667	18403	10.05	2.500	2.6
Z	(3+4)-II-1	--	--	2993	--	17821	19915	17821	10.05	2.500	6.0

Pilastro : 2 [202 , 302]

Sez. R: By= 50.0 cm Bz=30.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$v_{max}=N/(fcd*A)=0.05 \leq 0.65$ [Comb. (3+4)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(+)	-8993	3974	130	8621	13857	8621	13857	2.6
Testa	(3+4)-I-1(+)	-7160	3013	-8986	8408	13613	8408	13613	1.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	6585	--	18255	34667	18255	10.05	2.500	2.8
Z	(3+4)-II-1	--	--	2586	--	17677	19915	17677	10.05	2.500	6.8

Pilastro : 3 [3 , 103]

Sez. R: By= 50.0 cm Bz=30.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Non verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00	Sezione non verificata

$v_{max}=N/(fcd*A)=0.162 \leq 0.65$ [Comb. (3+4)-I-1(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-18816	-1012	-28259	9742	15076	9742	15076	0.38
Sezione non verificata : Sezione non verificata									

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Testa	(3+4)-I-3(+)	-17691	-490	17650	9616	14944	9616	14944	0.75
Sezione non verificata : Sezione non verificata									

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	19397	--	19895	23111	19895	6.70	2.500	1.0
Z	(3+4)-II-2	--	--	1064	15402	--	--	15402	6.70	2.500	14

Pilastro : 3 [103 , 203]

Sez. R: By= 50.0 cm Bz=30.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$v_{max}=N/(fcd*A)=0.056 \leq 0.65$ [Comb. (3+4)-II-1(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-9372	-799	-12794	8665	13907	8665	13907	1.1
Testa	(3+4)-II-1(+)	-9003	3994	973	8623	13858	8623	13858	2.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	7034	--	18518	34667	18518	10.05	2.500	2.6
Z	(3+4)-II-1	--	--	3203	--	17820	19915	17820	10.05	2.500	5.6

Pilastro : 3 [203 , 303]

Sez. R: By= 50.0 cm Bz=30.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$v_{max}=N/(fcd*A)=0.05 \leq 0.65$ [Comb. (3+4)-II-1(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(+)	-8981	4271	1560	8620	13856	8620	13856	2.3
Testa	(3+4)-II-1(+)	-8569	6502	4038	8572	13801	8572	13801	1.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	6542	--	18370	34667	18370	10.05	2.500	2.8
Z	(3+4)-II-1	--	--	2760	--	17675	19915	17675	10.05	2.500	6.4

Pilastro : 4 [4 , 104]

Sez. R: By= 50.0 cm Bz=30.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 :**Non verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00	

$v_{max}=N/(fcd*A)=0.174 \leq 0.65$ [Comb. (3+4)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(+)	-27276	3640	20056	10681	15957	10681	15957	0.50
Sezione non verificata : Sezione non verificata									

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Testa	(3+4)-I-1(+)	-26151	-259	-12247	10558	15848	10558	15848	1.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	14199	--	21130	23111	21130	6.70	2.500	1.5
Z	(3+4)-II-1	--	--	3770	15402	--	--	15402	6.70	2.500	4.1

Pilastro : 4 [104 , 204]

Sez. R: By= 50.0 cm Bz=30.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00	

$v_{max}=N/(fcd*A)=0.056 \leq 0.65$ [Comb. (3+4)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-6750	-4767	11193	8360	13557	8360	13557	0.75
	Sezione non verificata : Sezione non verificata								
Testa	(3+4)-I-3(+)	-5737	2494	4427	8242	13419	8242	13419	2.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	6283	--	18405	34667	18405	10.05	2.500	2.9
Z	(3+4)-II-1	--	--	4247	--	17812	19915	17812	10.05	2.500	4.2

Pilastro : 4 [204 , 304]

Sez. R: By= 50.0 cm Bz=30.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$v_{max}=N/(fcd*A)=0.05 \leq 0.65$ [Comb. (3+4)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(+)	-5750	2792	4367	8243	13421	8243	13421	2.3
Testa	(3+4)-II-1(+)	-8502	6829	-720	8564	13792	8564	13792	1.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	5737	--	18256	34667	18256	10.05	2.500	3.2
Z	(3+4)-II-1	--	--	3724	--	17666	19915	17666	10.05	2.500	4.7

Pilastro : 5 [28 , 128]

Sez. R: By= 50.0 cm Bz=30.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$v_{max}=N/(fcd*A)=0.152 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-20562	-2834	-13005	9938	15278	9938	15278	1.1
Testa	(3+4)-II-2(+)	-25837	-4730	7225	10523	15818	10523	15818	1.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	9172	--	20150	23111	20150	6.70	2.500	2.2
Z	(3+4)-II-2	--	--	4423	15402	--	--	15402	6.70	2.500	3.5

Pilastro : 5 [128 , 228]

Sez. R: By= 50.0 cm Bz=30.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$v_{max}=N/(fcd*A)=0.048 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(-)	-8557	6097	-7099	8571	13799	8571	13799	1.2
Testa	(3+4)-II-2(+)	-7545	-2088	2659	8453	13664	8453	13664	3.6

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-II-2	--	--	4411	--	18399	34667	18399	10.05	2.500	4.2
Z	(3+4)-II-2	--	--	3920	--	17616	19915	17616	10.05	2.500	4.5

Pilastro : 5 [228 , 328]

Sez. R: By= 50.0 cm Bz=30.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$v_{max}=N/(fcd*A)=0.042 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(+)	-7531	-2438	3402	8451	13663	8451	13663	2.9
Testa	(3+4)-II-2(+)	-7118	-5260	6526	8403	13607	8403	13607	1.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-II-2	--	--	4292	--	18249	34667	18249	10.05	2.500	4.3
Z	(3+4)-II-2	--	--	3723	--	17473	19915	17473	10.05	2.500	4.7

Pilastro : 6 [27 , 127]

Sez. R: By= 50.0 cm Bz=30.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 8.04	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 8.04	Afz = 2.01

$v_{max}=N/(fcd*A)=0.168 \leq 0.65$ [Comb. (3+4)-I-1(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-29758	2748	14244	15943	23090	15943	23090	1.5
Testa	(3+4)-I-1(+)	-28633	-2493	-9001	15868	22996	15868	22996	2.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
-----	----	-------	-------	---	-------	------	------	-----	-------	--------	----

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	9873	--	21439	23111	21439	6.70	2.500	2.2
Z	(3+4)-II-2	--	--	4553	17707	--	--	17707	6.70	2.500	3.9

Pilastro : 6 [127 , 227]

Sez. R: By= 50.0 cm Bz=30.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 8.04	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 8.04	Afz = 2.01

$$v_{max}=N/(fcd*A)=0.066 \leq 0.65 \quad [\text{Comb. (3+4)-I-1(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(-)	-10680	7286	-4712	14177	21405	14177	21405	1.8
Testa	(3+4)-II-2(+)	-9668	-3481	2352	14063	21312	14063	21312	3.9

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-II-1	--	--	3864	--	18453	34667	18453	10.05	2.500	4.8
Z	(3+4)-II-2	--	--	4756	--	17913	19915	17913	10.05	2.500	3.8

Pilastro : 6 [227 , 327]

Sez. R: By= 50.0 cm Bz=30.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 8.04	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 8.04	Afz = 2.01

$$v_{max}=N/(fcd*A)=0.06 \leq 0.65 \quad [\text{Comb. (3+4)-I-1(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(+)	-9659	-3952	2886	14062	21312	14062	21312	3.3
Testa	(3+4)-II-2(+)	-9247	-7742	5136	14016	21274	14016	21274	1.6

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-II-1	--	--	3766	--	18306	34667	18306	10.05	2.500	4.9
Z	(3+4)-II-2	--	--	4606	--	17770	19915	17770	10.05	2.500	3.9

Pilastro : 7 [26 , 126]

Sez. R: By= 50.0 cm Bz=30.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00	

$$v_{max}=N/(fcd*A)=0.159 \leq 0.65 \quad [\text{Comb. (3+4)-II-2(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-24400	3163	14300	10365	15677	10365	15677	0.75
Sezione non verificata : Sezione non verificata									
Testa	(3+4)-I-1(+)	-23275	-4180	-10941	10240	15566	10240	15566	1.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
Y	(3+4)-I-1	--	--	10984	--	20710	23111	20710	6.70	2.500	1.9
Z	(3+4)-II-2	--	--	3185	15402	--	--	15402	6.70	2.500	4.8

Pilastro : 7 [126 , 226]

Sez. R: By= 50.0 cm Bz=30.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$v_{max}=N/(fcd*A)=0.029 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-4270	3266	7789	8069	13216	8069	13216	1.4
Testa	(3+4)-I-3(+)	-3895	-286	2609	8025	13164	8025	13164	5.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	5085	--	17774	34667	17774	10.05	2.500	3.5
Z	(3+4)-II-2	--	--	1696	--	17139	19915	17139	10.05	2.500	10

Pilastro : 7 [226 , 326]

Sez. R: By= 50.0 cm Bz=30.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$v_{max}=N/(fcd*A)=0.023 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(+)	-3258	-188	-3387	7950	13074	7950	13074	4.2
Testa	(3+4)-I-1(+)	-2846	-1499	-6732	7901	13016	7901	13016	1.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	5003	--	17626	34667	17626	10.05	2.500	3.5
Z	(3+4)-II-2	--	--	1599	--	16997	19915	16997	10.05	2.500	11

Pilastro : 8 [29 , 129]

Sez. R: By= 50.0 cm Bz=30.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$v_{max}=N/(fcd*A)=0.152 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-16961	-2750	-12632	9533	14857	9533	14857	1.1
Testa	(3+4)-I-1(+)	-22587	-895	-9821	10164	15498	10164	15498	1.7

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	9991	--	20610	23111	20610	6.70	2.500	2.1
Z	(3+4)-I-1	--	--	1102	15402	--	--	15402	6.70	2.500	14

Pilastro : 8 [129 , 229]

Sez. R: By= 50.0 cm Bz=30.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$$v_{\max}=N/(fcd*A)=0.077 \leq 0.65 \quad [\text{Comb. (3+4)-II-2(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-2995	-1715	7629	7919	13037	7919	13037	1.6
Testa	(3+4)-II-1(+)	-1983	2436	-2801	7799	12875	7799	12875	2.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	5379	--	18770	34667	18770	10.05	2.500	3.5
Z	(3+4)-II-2	--	--	2557	--	18334	19915	18334	10.05	2.500	7.2

Pilastro : 8 [229 , 329]

Sez. R: By= 50.0 cm Bz=30.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$$v_{\max}=N/(fcd*A)=0.071 \leq 0.65 \quad [\text{Comb. (3+4)-II-2(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(+)	-1997	2597	-3592	7801	12877	7801	12877	2.4
Testa	(3+4)-II-1(+)	-1584	3897	-6916	7752	12809	7752	12809	1.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	5188	--	18621	34667	18621	10.05	2.500	3.6
Z	(3+4)-II-2	--	--	2293	--	18191	19915	18191	10.05	2.500	7.9

Pilastro : 9 [5 , 105]

Sez. R: By= 30.0 cm Bz=50.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$$v_{\max}=N/(fcd*A)=0.22 \leq 0.65 \quad [\text{Comb. (3+4)-I-3(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-23921	7553	8236	15630	10312	15630	10312	1.0
Testa	(3+4)-I-3(+)	-37740	-3804	7842	16923	11747	16923	11747	1.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	7519	15402	--	--	15402	6.70	2.500	2.0
Z	(3+4)-II-2	--	--	7508	--	21430	23111	21430	6.70	2.500	2.9

Pilastro : 9 [105 , 205]

Sez. R: By= 30.0 cm Bz=50.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.072 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-12855	-1936	-8085	14354	9066	14354	9066	1.1
Testa	(3+4)-II-2(+)	-7678	-6320	91	13682	8469	13682	8469	2.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	5457	--	18216	19915	18216	10.05	2.500	3.3
Z	(3+4)-II-2	--	--	6721	--	18419	34667	18419	10.05	2.500	2.7

Pilastr : 9 [205 , 305]

Sez. R: By= 30.0 cm Bz=50.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.067 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(+)	-7684	-7383	174	13683	8469	13683	8469	2.0
Testa	(3+4)-I-3(+)	-11421	1670	8511	14172	8902	14172	8902	1.0

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	5153	--	18074	19915	18074	10.05	2.500	3.5
Z	(3+4)-II-2	--	--	6455	--	18272	34667	18272	10.05	2.500	2.8

Pilastr : 10 [10 , 110]

Sez. R: By= 30.0 cm Bz=50.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	

$v_{max}=N/(fcd*A)=0.216 \leq 0.65$ [Comb. (3+4)-I-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(+)	-38234	10076	8777	16966	11789	16966	11789	0.75
Sezione non verificata : Sezione non verificata									
Testa	(3+4)-I-1(+)	-37109	-3989	-7544	16867	11692	16867	11692	1.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	7219	15402	--	--	15402	6.70	2.500	2.1
Z	(3+4)-II-2	--	--	7967	--	21108	23111	21108	6.70	2.500	2.6

Pilastr : 10 [110 , 210]

Sez. R: By= 30.0 cm Bz=50.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2,

qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.069 \leq 0.65$ [Comb. (3+4)-I-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-12302	5393	8170	14285	9003	14285	9003	1.0
Testa	(3+4)-I-1(+)	-11290	-5126	-3934	14156	8887	14156	8887	1.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	5520	--	18139	19915	18139	10.05	2.500	3.3
Z	(3+4)-II-2	--	--	7122	--	18235	34667	18235	10.05	2.500	2.6

Pilastro : 10 [210 , 310]

Sez. R: By= 30.0 cm Bz=50.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2,

qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	Sezione non verificata

$v_{max}=N/(fcd*A)=0.063 \leq 0.65$ [Comb. (3+4)-I-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(+)	-11273	-5902	-4428	14154	8885	14154	8885	1.6
Testa	(3+4)-I-1(+)	-10861	-9165	-8416	14101	8837	14101	8837	0.75
Sezione non verificata : Sezione non verificata									

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	5005	--	17995	19915	17995	10.05	2.500	3.6
Z	(3+4)-II-2	--	--	6648	--	18093	34667	18093	10.05	2.500	2.7

Pilastro : 11 [14 , 114]

Sez. R: By= 30.0 cm Bz=50.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2,

qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	

$v_{max}=N/(fcd*A)=0.151 \leq 0.65$ [Comb. (3+4)-I-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-26711	12463	7518	15903	10619	15903	10619	0.75
Sezione non verificata : Sezione non verificata									
Testa	(3+4)-I-1(+)	-25586	-6959	-5088	15793	10495	15793	10495	1.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	5483	15402	--	--	15402	6.70	2.500	2.8
Z	(3+4)-II-2	--	--	9974	--	20293	23111	20293	6.70	2.500	2.0

Pilastro : 11 [114 , 214]

Sez. R: By= 30.0 cm Bz=50.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2,

qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$$v_{\max} = N / (f_{cd} \cdot A) = 0.047 \leq 0.65 \quad [\text{Comb. (3+4)-I-1(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-8381	5018	5848	13776	8550	13776	8550	1.4
Testa	(3+4)-I-3(+)	1000	1864	2317	12378	7444	12378	7444	3.0

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	4147	--	17592	19915	17592	10.05	2.500	4.2
Z	(3+4)-II-2	--	--	5073	--	18135	34667	18135	10.05	2.500	3.6

Pilastro : 11 [214 , 314]

Sez. R: By= 30.0 cm Bz=50.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2,

qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$$v_{\max} = N / (f_{cd} \cdot A) = 0.041 \leq 0.65 \quad [\text{Comb. (3+4)-I-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(+)	-7353	-2429	-3363	13639	8431	13639	8431	2.6
Testa	(3+4)-I-1(+)	-6941	-4540	-6242	13583	8383	13583	8383	1.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	3729	--	17448	19915	17448	10.05	2.500	4.7
Z	(3+4)-II-2	--	--	4657	--	17987	34667	17987	10.05	2.500	3.9

Pilastro : 12 [18 , 118]

Sez. R: By= 30.0 cm Bz=50.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2,

qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	

$$v_{\max} = N / (f_{cd} \cdot A) = 0.178 \leq 0.65 \quad [\text{Comb. (3+4)-I-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-22459	-15134	1912	15486	10150	15486	10150	0.75
Sezione non verificata : Sezione non verificata									
Testa	(3+4)-I-3(+)	-16006	7035	3100	14743	9425	14743	9425	1.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	5132	15402	--	--	15402	6.70	2.500	3.0
Z	(3+4)-II-1	--	--	9950	--	20427	23111	20427	6.70	2.500	2.1

Pilastro : 12 [118 , 218]

Sez. R: By= 30.0 cm Bz=50.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2,

qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$$v_{\max} = N / (f_{cd} \cdot A) = 0.044 \leq 0.65 \quad [\text{Comb. (3+4)-II-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-7792	-9095	350	13698	8482	13698	8482	1.6
Testa	(3+4)-I-1(+)	-6632	-1518	-2841	13541	8347	13541	8347	3.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	3939	--	17489	19915	17489	10.05	2.500	4.4
Z	(3+4)-II-1	--	--	5228	--	18288	34667	18288	10.05	2.500	3.5

Pilastro : 12 [218 , 318]

Sez. R: By= 30.0 cm Bz=50.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2,

qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$$v_{\max} = N / (f_{cd} \cdot A) = 0.038 \leq 0.65 \quad [\text{Comb. (3+4)-II-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(+)	-6619	-1744	-3187	13540	8345	13540	8345	2.9
Testa	(3+4)-I-1(+)	-6206	-2702	-5983	13484	8297	13484	8297	1.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	3587	--	17345	19915	17345	10.05	2.500	4.8
Z	(3+4)-II-1	--	--	4849	--	18139	34667	18139	10.05	2.500	3.7

Pilastro : 13 [30 , 130]

Sez. R: By= 30.0 cm Bz=50.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2,

qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$$v_{\max} = N / (f_{cd} \cdot A) = 0.156 \leq 0.65 \quad [\text{Comb. (3+4)-I-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(-)	-16448	12449	-2265	14796	9475	14796	9475	1.1
Testa	(3+4)-I-3(+)	-8563	-6347	3731	13800	8571	13800	8571	1.6

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	4688	15402	--	--	15402	6.70	2.500	3.3
Z	(3+4)-II-2	--	--	7477	--	19550	23111	19550	6.70	2.500	2.6

Pilastro : 13 [130 , 230]

Sez. R: By= 30.0 cm Bz=50.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2,

qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$$v_{\max} = N / (f_{cd} \cdot A) = 0.046 \leq 0.65 \quad [\text{Comb. (3+4)-I-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
------	----	---	----	----	------	------	------	------	----

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-8273	5897	5188	13762	8538	13762	8538	1.4
Testa	(3+4)-II-1(+)	-3805	3723	-1394	13151	8014	13151	8014	3.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	3373	--	17576	19915	17576	10.05	2.500	5.2
Z	(3+4)-II-2	--	--	5237	--	18091	34667	18091	10.05	2.500	3.5

Pilastro : 13 [230 , 330]

Sez. R: By= 30.0 cm Bz=50.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.041 \leq 0.65$ [Comb. (3+4)-I-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(+)	-3814	4124	-1609	13153	8016	13153	8016	2.8
Testa	(3+4)-I-1(+)	-6825	-4501	-4879	13568	8369	13568	8369	1.6

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	3117	--	17432	19915	17432	10.05	2.500	5.6
Z	(3+4)-II-2	--	--	4906	--	17942	34667	17942	10.05	2.500	3.7

Pilastro : 14 [25 , 125]

Sez. R: By= 30.0 cm Bz=50.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.121 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-6148	-9598	2088	13476	8290	13476	8290	1.3
Testa	(3+4)-I-3(+)	-17789	-3624	4328	14956	9627	14956	9627	2.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	4020	14781	--	--	14781	6.70	2.500	3.7
Z	(3+4)-II-2	--	--	6049	--	20277	23111	20277	6.70	2.500	3.4

Pilastro : 14 [125 , 225]

Sez. R: By= 30.0 cm Bz=50.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.046 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(-)	-8283	6748	-3153	13763	8539	13763	8539	1.7

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Testa	(3+4)-II-2(+)	-7271	-3648	1063	13628	8421	13628	8421	3.7

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	2240	--	17386	19915	17386	10.05	2.500	7.8
Z	(3+4)-II-2	--	--	4730	--	18359	34667	18359	10.05	2.500	3.9

Pilastro : 14 [225 , 325]

Sez. R: By= 30.0 cm Bz=50.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.041 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(+)	-7265	-4443	1250	13627	8420	13627	8420	3.0
Testa	(3+4)-II-2(+)	-6853	-7796	2759	13571	8372	13571	8372	1.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	2189	--	17244	19915	17244	10.05	2.500	7.9
Z	(3+4)-II-2	--	--	4663	--	18211	34667	18211	10.05	2.500	3.9

Pilastro : 15 [24 , 124]

Sez. R: By= 30.0 cm Bz=50.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.168 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-28721	-13140	612	16096	10839	16096	10839	1.3
Testa	(3+4)-I-3(+)	-28540	4067	4856	16078	10819	16078	10819	2.0

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	4008	15402	--	--	15402	6.70	2.500	3.8
Z	(3+4)-II-1	--	--	8250	--	21340	23111	21340	6.70	2.500	2.6

Pilastro : 15 [124 , 224]

Sez. R: By= 30.0 cm Bz=50.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.065 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-11211	-7825	-3161	14146	8878	14146	8878	1.5
Testa	(3+4)-II-2(+)	-9979	-4866	887	13986	8735	13986	8735	3.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	2189	--	18022	19915	18022	10.05	2.500	8.2
Z	(3+4)-II-1	--	--	5992	--	18786	34667	18786	10.05	2.500	3.1

Pilastro : 15 [224 , 324]

Sez. R: By= 30.0 cm Bz=50.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.059 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(+)	-9980	-5784	1024	13986	8736	13986	8736	2.5
Testa	(3+4)-II-2(+)	-9567	-9645	2173	13933	8688	13933	8688	1.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	2116	--	17880	19915	17880	10.05	2.500	8.5
Z	(3+4)-II-1	--	--	5883	--	18638	34667	18638	10.05	2.500	3.2

Pilastro : 16 [19 , 119]

Sez. R: By= 30.0 cm Bz=50.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.196 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-34732	-6824	-7417	16655	11481	16655	11481	1.2
Testa	(3+4)-I-3(+)	-33607	2593	6751	16553	11369	16553	11369	1.7

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	5831	15402	--	--	15402	6.70	2.500	2.6
Z	(3+4)-II-1	--	--	7451	--	21181	23111	21181	6.70	2.500	2.8

Pilastro : 16 [119 , 219]

Sez. R: By= 30.0 cm Bz=50.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.064 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-11367	2667	-6825	14165	8896	14165	8896	1.3
Testa	(3+4)-II-1(+)	-7136	5984	282	13610	8405	13610	8405	2.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
Y	(3+4)-I-3	--	--	4359	--	18009	19915	18009	10.05	2.500	4.1
Z	(3+4)-II-1	--	--	6393	--	18340	34667	18340	10.05	2.500	2.9

Pilastro : 16 [219 , 319]

Sez. R: $B_y = 30.0 \text{ cm}$ $B_z = 50.0 \text{ cm}$ $L = 110.0 \text{ cm}$ $L_n = 110.0 \text{ cm}$

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{\max} = N/(fcd \cdot A) = 0.058 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(+)	-7138	7000	398	13610	8406	13610	8406	2.1
Testa	(3+4)-I-3(+)	-9938	5601	6953	13981	8731	13981	8731	1.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	4233	--	17867	19915	17867	10.05	2.500	4.2
Z	(3+4)-II-1	--	--	6238	--	18192	34667	18192	10.05	2.500	2.9

Pilastro : 17 [15 , 115]

Sez. R: $B_y = 30.0 \text{ cm}$ $B_z = 50.0 \text{ cm}$ $L = 300.0 \text{ cm}$ $L_n = 300.0 \text{ cm}$

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{\max} = N/(fcd \cdot A) = 0.151 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-22569	-14159	-2491	15497	10162	15497	10162	1.0
Testa	(3+4)-I-3(+)	-25649	4543	5373	15799	10502	15799	10502	1.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	5552	15402	--	--	15402	6.70	2.500	2.8
Z	(3+4)-II-1	--	--	9089	--	20443	23111	20443	6.70	2.500	2.2

Pilastro : 17 [115 , 215]

Sez. R: $B_y = 30.0 \text{ cm}$ $B_z = 50.0 \text{ cm}$ $L = 270.0 \text{ cm}$ $L_n = 270.0 \text{ cm}$

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{\max} = N/(fcd \cdot A) = 0.038 \leq 0.65$ [Comb. (3+4)-II-1(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-6521	1624	-5481	13526	8334	13526	8334	1.6
Testa	(3+4)-I-3(+)	-5509	1503	2784	13388	8215	13388	8215	3.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	3808	--	17332	19915	17332	10.05	2.500	4.6
Z	(3+4)-II-1	--	--	4535	--	18141	34667	18141	10.05	2.500	4.0

Pilastro : 17 [215 , 315]

Sez. R: By= 30.0 cm Bz=50.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$$v_{\max} = N / (f_{cd} \cdot A) = 0.032 \leq 0.65 \quad [\text{Comb. (3+4)-II-1(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(+)	-5504	1506	3135	13387	8214	13387	8214	2.9
Testa	(3+4)-I-3(+)	-5092	2894	5974	13331	8166	13331	8166	1.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	3627	--	17190	19915	17190	10.05	2.500	4.7
Z	(3+4)-II-1	--	--	4347	--	17994	34667	17994	10.05	2.500	4.1

Pilastro : 18 [11 , 111]

Sez. R: By= 30.0 cm Bz=50.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$$v_{\max} = N / (f_{cd} \cdot A) = 0.154 \leq 0.65 \quad [\text{Comb. (3+4)-I-3(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(-)	-23107	14360	1186	15550	10221	15550	10221	1.1
Testa	(3+4)-I-3(+)	-26198	-5166	5724	15853	10563	15853	10563	1.6

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	6050	15402	--	--	15402	6.70	2.500	2.5
Z	(3+4)-II-2	--	--	9129	--	20521	23111	20521	6.70	2.500	2.2

Pilastro : 18 [111 , 211]

Sez. R: By= 30.0 cm Bz=50.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :Verificato

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$$v_{\max} = N / (f_{cd} \cdot A) = 0.042 \leq 0.65 \quad [\text{Comb. (3+4)-I-3(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-7576	-1647	-5915	13669	8457	13669	8457	1.5
Testa	(3+4)-I-3(+)	-6563	912	3011	13532	8338	13532	8338	3.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	4136	--	17479	19915	17479	10.05	2.500	4.2
Z	(3+4)-II-2	--	--	4561	--	18226	34667	18226	10.05	2.500	4.0

Pilastro : 18 [211 , 311]

Sez. R: By= 30.0 cm Bz=50.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.037 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(+)	-6557	1094	3388	13531	8338	13531	8338	2.8
Testa	(3+4)-I-3(+)	-6144	1864	6429	13475	8289	13475	8289	1.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	3907	--	17337	19915	17337	10.05	2.500	4.4
Z	(3+4)-II-2	--	--	4344	--	18079	34667	18079	10.05	2.500	4.2

Pilastro : 19 [33 , 133]

Sez. R: By= 30.0 cm Bz=50.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	Sezione non verificata

$v_{max}=N/(fcd*A)=0.073 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-9718	-2195	11047	13952	8705	13952	8705	0.75
	Sezione non verificata : Sezione non verificata								
Testa	(3+4)-I-1(-)	-8593	-823	-9350	13804	8575	13804	8575	0.75
	Sezione non verificata : Sezione non verificata								

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	9174	13539	--	--	13539	6.70	2.500	1.5
Z	(3+4)-II-2	--	--	5470	--	18747	23111	18747	6.70	2.500	3.4

Pilastro : 20 [32 , 132]

Sez. R: By= 30.0 cm Bz=50.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	Sezione non verificata

$v_{max}=N/(fcd*A)=0.076 \leq 0.65$ [Comb. (3+4)-I-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-13534	5063	9307	14439	9144	14439	9144	0.75
	Sezione non verificata : Sezione non verificata								
Testa	(3+4)-I-3(+)	-9084	-681	10176	13869	8632	13869	8632	0.75
	Sezione non verificata : Sezione non verificata								

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	9111	13606	--	--	13606	6.70	2.500	1.5
Z	(3+4)-II-2	--	--	5583	--	18813	23111	18813	6.70	2.500	3.4

Pilastro : 21 [34 , 134]

Sez. R: By= 30.0 cm Bz=50.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	Sezione non verificata

$$v_{\max} = N / (f_{cd} \cdot A) = 0.074 \leq 0.65 \quad [\text{Comb. (3+4)-I-3(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-10183	-3923	10056	14013	8759	14013	8759	0.75
	Sezione non verificata : Sezione non verificata								
Testa	(3+4)-I-1(+)	-9058	707	-9361	13866	8629	13866	8629	0.75
	Sezione non verificata : Sezione non verificata								

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	8356	13602	--	--	13602	6.70	2.500	1.6
Z	(3+4)-II-1	--	--	5548	--	18795	23111	18795	6.70	2.500	3.4

Pilastro : 22 [31 , 131]

Sez. R: By= 30.0 cm Bz=50.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02	Sezione non verificata

$$v_{\max} = N / (f_{cd} \cdot A) = 0.077 \leq 0.65 \quad [\text{Comb. (3+4)-I-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(+)	-10617	-4716	-9081	14069	8809	14069	8809	0.75
	Sezione non verificata : Sezione non verificata								
Testa	(3+4)-I-3(+)	-9492	725	9238	13923	8679	13923	8679	0.75
	Sezione non verificata : Sezione non verificata								

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	8236	13661	--	--	13661	6.70	2.500	1.7
Z	(3+4)-II-1	--	--	5687	--	18869	23111	18869	6.70	2.500	3.3

Pilastro : 23 [6 , 106]

Sez. R: By= 30.0 cm Bz=90.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	

$$v_{\max} = N / (f_{cd} \cdot A) = 0.117 \leq 0.65 \quad [\text{Comb. (3+4)-I-3(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(+)	-26811	43455	5044	45004	16374	45004	16374	0.75
	Sezione non verificata : Sezione non verificata								
Testa	(3+4)-I-1(+)	-20490	-4472	-12460	43455	15651	43455	15651	1.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	13249	24843	--	--	24843	10.05	2.500	1.9
Z	(3+4)-II-2	--	--	16839	--	35769	64170	35769	10.05	2.500	2.1

Pilastro : 23 [106 , 206]

Sez. R: By= 30.0 cm Bz=90.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	

$$v_{\max} = N / (f_{cd} \cdot A) = 0.053 \leq 0.65 \quad [\text{Comb. (3+4)-I-3(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-8051	-3778	14820	40257	14202	40257	14202	0.75
	Sezione non verificata : Sezione non verificata								
Testa	(3+4)-I-1(+)	-6228	3182	-11036	39771	13987	39771	13987	1.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	12415	22891	--	--	22891	10.05	2.500	1.8
Z	(3+4)-II-2	--	--	10021	--	33080	64170	33080	10.05	2.500	3.3

Pilastro : 23 [206 , 306]

Sez. R: By= 30.0 cm Bz=90.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05

$$v_{\max} = N / (f_{cd} \cdot A) = 0.027 \leq 0.65 \quad [\text{Comb. (3+4)-II-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(-)	-4197	-6344	-1961	39224	13746	39224	13746	5.1
Testa	(3+4)-I-1(+)	-6889	-2390	-9332	39947	14065	39947	14065	1.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	11967	22834	--	--	22834	10.05	2.500	1.9
Z	(3+4)-II-1	--	--	5786	--	33076	64170	33076	10.05	2.500	5.7

Pilastro : 23 [306 , 406]

Sez. R: By= 30.0 cm Bz=50.0 cm L=170.0 cm Ln=170.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$$v_{\max} = N / (f_{cd} \cdot A) = 0.03 \leq 0.65 \quad [\text{Comb. (3+4)-I-3(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(+)	-4973	4547	1374	13314	8152	13314	8152	2.8
Testa	(3+4)-II-1(+)	-4335	11935	-2614	13226	8077	13226	8077	1.0

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	5764	--	16579	19915	16579	10.05	2.500	2.9
Z	(3+4)-II-1	--	--	7180	--	17876	34667	17876	10.05	2.500	2.5

Pilastro : 24 [8 , 108]

Sez. R: By= 30.0 cm Bz=90.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastri-Exist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	

$$v_{\max} = N / (f_{cd} \cdot A) = 0.109 \leq 0.65 \quad [\text{Comb. (3+4)-II-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-34779	-47298	-4133	46887	17274	46887	17274	0.75
	Sezione non verificata : Sezione non verificata								
Testa	(3+4)-I-3(+)	-31412	-3517	10749	46100	16896	46100	16896	1.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	12421	26318	--	--	26318	10.05	2.500	2.1
Z	(3+4)-II-2	--	--	19491	--	36345	64170	36345	10.05	2.500	1.9

Pilastro : 24 [108 , 208]

Sez. R: By= 30.0 cm Bz=90.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastri-Exist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	Sezione non verificata

$$v_{\max} = N / (f_{cd} \cdot A) = 0.069 \leq 0.65 \quad [\text{Comb. (3+4)-II-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-18704	-6039	15553	43008	15445	43008	15445	0.75
	Sezione non verificata : Sezione non verificata								
Testa	(3+4)-I-1(+)	-16882	-6039	-15676	42548	15234	42548	15234	0.75
	Sezione non verificata : Sezione non verificata								

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	15398	24329	--	--	24329	10.05	2.500	1.6
Z	(3+4)-II-1	--	--	10416	--	35048	64170	35048	10.05	2.500	3.4

Pilastro : 24 [208 , 308]

Sez. R: By= 30.0 cm Bz=90.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastri-Exist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05

$$v_{\max} = N / (f_{cd} \cdot A) = 0.05 \leq 0.65 \quad [\text{Comb. (3+4)-II-2(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-12667	-6292	5541	41467	14744	41467	14744	2.9
Testa	(3+4)-II-2(+)	-15418	-12138	1227	42175	15064	42175	15064	3.9

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	9046	23906	--	--	23906	10.05	2.500	2.6
Z	(3+4)-II-1	--	--	5817	--	33559	64170	33559	10.05	2.500	5.8

Pilastro : 24 [308 , 408]

Sez. R: By= 30.0 cm Bz=50.0 cm L=170.0 cm Ln=170.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$$v_{\max} = N / (f_{cd} \cdot A) = 0.065 \leq 0.65 \quad [\text{Comb. (3+4)-II-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(+)	-11606	5745	-325	14196	8923	14196	8923	2.8
Testa	(3+4)-I-3(+)	-10957	7398	7684	14113	8848	14113	8848	1.0

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	5861	--	18040	19915	18040	10.05	2.500	3.1
Z	(3+4)-II-2	--	--	5413	--	18340	34667	18340	10.05	2.500	3.4

Pilastro : 25 [9 , 109]

Sez. R: By= 30.0 cm Bz=90.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	

$$v_{\max} = N / (f_{cd} \cdot A) = 0.114 \leq 0.65 \quad [\text{Comb. (3+4)-I-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(+)	-36213	26661	14953	47217	17435	47217	17435	0.75
Sezione non verificata : Sezione non verificata									
Testa	(3+4)-I-3(+)	-21527	-6174	12673	43712	15770	43712	15770	1.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	13398	24983	--	--	24983	10.05	2.500	1.9
Z	(3+4)-II-2	--	--	17458	--	35570	64170	35570	10.05	2.500	2.0

Pilastro : 25 [109 , 209]

Sez. R: By= 30.0 cm Bz=90.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 10.05	Afz = 2.01	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 10.05	Afz = 2.01	

$$v_{\max} = N / (f_{cd} \cdot A) = 0.053 \leq 0.65 \quad [\text{Comb. (3+4)-II-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-9093	-6016	-14932	54136	14596	54136	14596	0.75
Sezione non verificata : Sezione non verificata									
Testa	(3+4)-I-3(+)	-7271	7363	11112	53434	14447	53434	14447	1.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	12537	24024	--	--	24024	10.05	2.500	1.9
Z	(3+4)-II-2	--	--	10962	--	32929	64170	32929	10.05	2.500	3.0

Pilastro : 25 [209 , 309]

Sez. R: By= 30.0 cm Bz=90.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05

$v_{max}=N/(fcd*A)=0.028 \leq 0.65$ [Comb. (3+4)-II-1(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(-)	-4308	-6735	1495	39254	13759	39254	13759	5.4
Testa	(3+4)-I-3(+)	-7732	1858	9894	40172	14164	40172	14164	1.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	13750	22948	--	--	22948	10.05	2.500	1.7
Z	(3+4)-II-1	--	--	4753	--	33098	64170	33098	10.05	2.500	7.0

Pilastr : 25 [309 , 409]

Sez. R: By= 30.0 cm Bz=50.0 cm L=170.0 cm Ln=170.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.03 \leq 0.65$ [Comb. (3+4)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(+)	-5369	5641	-1611	13369	8199	13369	8199	2.2
Testa	(3+4)-I-3(+)	-1247	8086	5782	12753	7712	12753	7712	1.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	5658	--	16684	19915	16684	10.05	2.500	2.9
Z	(3+4)-II-1	--	--	4697	--	17934	34667	17934	10.05	2.500	3.8

Pilastr : 26 [20 , 120]

Sez. R: By= 30.0 cm Bz=90.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	

$v_{max}=N/(fcd*A)=0.125 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(+)	-26946	-43367	3889	45037	16390	45037	16390	0.75
	Sezione non verificata : Sezione non verificata								
Testa	(3+4)-I-1(+)	-26510	-1290	-9275	44931	16340	44931	16340	2.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	9376	25656	--	--	25656	10.05	2.500	2.7
Z	(3+4)-II-1	--	--	17037	--	35789	64170	35789	10.05	2.500	2.1

Pilastr : 26 [120 , 220]

Sez. R: By= 30.0 cm Bz=90.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2,

qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05

$v_{max}=N/(fcd*A)=0.059 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-9075	-1736	10810	40528	14322	40528	14322	1.4
Testa	(3+4)-I-1(+)	-7252	-4280	-7900	40044	14108	40044	14108	1.9

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	8801	23029	--	--	23029	10.05	2.500	2.6
Z	(3+4)-II-2	--	--	10065	--	34578	64170	34578	10.05	2.500	3.4

Pilastro : 26 [220 , 320]

Sez. R: By= 30.0 cm Bz=90.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2,

qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05

$v_{max}=N/(fcd*A)=0.032 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-2549	4887	-1304	38776	13550	38776	13550	6.9
Testa	(3+4)-I-1(+)	-4581	-1768	-6223	39328	13792	39328	13792	2.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	6990	22522	--	--	22522	10.05	2.500	3.2
Z	(3+4)-II-2	--	--	6159	--	33311	64170	33311	10.05	2.500	5.4

Pilastro : 26 [320 , 420]

Sez. R: By= 30.0 cm Bz=50.0 cm L=170.0 cm Ln=170.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2,

qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.04 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	653	2442	1384	12436	7485	12436	7485	3.7
Testa	(3+4)-II-2(+)	-6540	-12494	-656	13529	8336	13529	8336	1.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	4633	--	16631	19915	16631	10.05	2.500	3.6
Z	(3+4)-II-2	--	--	8432	--	18198	34667	18198	10.05	2.500	2.2

Pilastro : 27 [21 , 121]

Sez. R: By= 30.0 cm Bz=90.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2,

qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	

$$v_{\max}=N/(fcd \cdot A)=0.133 \leq 0.65 \quad [\text{Comb. (3+4)-II-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(+)	-42516	-50294	3463	48616	18136	48616	18136	0.75
	Sezione non verificata : Sezione non verificata								
Testa	(3+4)-I-1(+)	-33720	4840	-8661	46641	17155	46641	17155	2.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	9182	26629	--	--	26629	10.05	2.500	2.9
Z	(3+4)-II-1	--	--	26006	--	38125	64170	38125	10.05	2.500	1.5

Pilastro : 27 [121 , 221]

Sez. R: By= 30.0 cm Bz=90.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05

$$v_{\max}=N/(fcd \cdot A)=0.072 \leq 0.65 \quad [\text{Comb. (3+4)-II-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-22399	-6196	11923	43928	15870	43928	15870	1.4
Testa	(3+4)-I-1(+)	-20577	3995	-11364	43477	15661	43477	15661	1.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	11298	24828	--	--	24828	10.05	2.500	2.2
Z	(3+4)-II-1	--	--	12519	--	35221	64170	35221	10.05	2.500	2.8

Pilastro : 27 [221 , 321]

Sez. R: By= 30.0 cm Bz=90.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05

$$v_{\max}=N/(fcd \cdot A)=0.053 \leq 0.65 \quad [\text{Comb. (3+4)-II-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-16528	5707	3155	42458	15193	42458	15193	4.9
Testa	(3+4)-II-1(+)	-16390	10689	-664	42423	15177	42423	15177	4.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	4815	24035	--	--	24035	10.05	2.500	5.0
Z	(3+4)-I-1	--	--	3835	--	34227	64170	34227	10.05	2.500	8.9

Pilastro : 27 [321 , 421]

Sez. R: By= 30.0 cm Bz=50.0 cm L=170.0 cm Ln=170.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$$v_{\max}=N/(fcd \cdot A)=0.061 \leq 0.65 \quad [\text{Comb. (3+4)-I-1(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(+)	-10761	-3361	-600	14088	8826	14088	8826	4.9
Testa	(3+4)-I-3(+)	-7280	-6962	5189	13629	8422	13629	8422	1.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	5518	--	17924	19915	17924	10.05	2.500	3.2
Z	(3+4)-II-2	--	--	5250	--	18679	34667	18679	10.05	2.500	3.6

Pilastro : 28 [22 , 122]

Sez. R: By= 30.0 cm Bz=90.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	

$v_{max}=N/(fcd*A)=0.149 \leq 0.65$ [Comb. (3+4)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(+)	-47349	-50306	2859	49580	18669	49580	18669	0.75
	Sezione non verificata : Sezione non verificata								
Testa	(3+4)-I-3(+)	-36216	5030	9032	47218	17435	47218	17435	2.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	9192	26966	--	--	26966	10.05	2.500	2.9
Z	(3+4)-II-1	--	--	26065	--	38850	64170	38850	10.05	2.500	1.5

Pilastro : 28 [122 , 222]

Sez. R: By= 30.0 cm Bz=90.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05

$v_{max}=N/(fcd*A)=0.077 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-23731	-6240	-11551	44256	16023	44256	16023	1.5
Testa	(3+4)-I-3(+)	-21909	4151	9790	43807	15814	43807	15814	1.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	10304	25008	--	--	25008	10.05	2.500	2.4
Z	(3+4)-II-1	--	--	11387	--	34876	64170	34876	10.05	2.500	3.1

Pilastro : 28 [222 , 322]

Sez. R: By= 30.0 cm Bz=90.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05

$v_{max}=N/(fcd*A)=0.058 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Piede	(3+4)-I-3(-)	-18639	5141	-3560	42992	15437	42992	15437	4.8
Testa	(3+4)-I-3(+)	-17896	-2789	5349	42805	15352	42805	15352	3.7

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	10421	24320	--	--	24320	10.05	2.500	2.3
Z	(3+4)-II-2	--	--	7439	--	34356	64170	34356	10.05	2.500	4.6

Pilastro : 28 [322 , 422]

Sez. R: By= 30.0 cm Bz=50.0 cm L=170.0 cm Ln=170.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.07 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-11429	2559	-3075	14174	8903	14174	8903	3.0
Testa	(3+4)-I-3(+)	-9481	-5959	6603	13921	8678	13921	8678	1.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	6545	--	17834	19915	17834	10.05	2.500	2.7
Z	I	--	--	6229	--	19192	34667	19192	10.05	2.500	3.1

Pilastro : 29 [23 , 123]

Sez. R: By= 30.0 cm Bz=90.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	

$v_{max}=N/(fcd*A)=0.116 \leq 0.65$ [Comb. (3+4)-I-1(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-28098	-50252	2847	45313	16521	45313	16521	0.75
Sezione non verificata : Sezione non verificata									
Testa	(3+4)-I-3(-)	-21434	-9255	5734	43690	15760	43690	15760	2.7

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	7610	24971	--	--	24971	10.05	2.500	3.3
Z	(3+4)-II-1	--	--	16957	--	35962	64170	35962	10.05	2.500	2.1

Pilastro : 29 [123 , 223]

Sez. R: By= 30.0 cm Bz=90.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05

$v_{max}=N/(fcd*A)=0.061 \leq 0.65$ [Comb. (3+4)-I-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-7775	-5984	-7404	40183	14169	40183	14169	2.0

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Testa	(3+4)-I-3(+)	-5952	10435	5851	39697	13954	39697	13954	2.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	6934	24437	--	--	24437	10.05	2.500	3.5
Z	(3+4)-II-2	--	--	14955	--	34204	64170	34204	10.05	2.500	2.3

Pilastro : 29 [223 , 323]

Sez. R: By= 30.0 cm Bz=90.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05

$v_{max}=N/(fcd*A)=0.035 \leq 0.65$ [Comb. (3+4)-I-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-5806	8765	2515	39657	13937	39657	13937	3.8
Testa	(3+4)-I-1(+)	-10585	-9923	-5837	40925	14500	40925	14500	2.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	6981	23333	--	--	23333	10.05	2.500	3.3
Z	(3+4)-II-2	--	--	8688	--	33158	64170	33158	10.05	2.500	3.8

Pilastro : 29 [323 , 423]

Sez. R: By= 30.0 cm Bz=50.0 cm L=170.0 cm Ln=170.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.035 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-297	-3423	997	12595	7598	12595	7598	3.3
Testa	(3+4)-II-2(+)	-5656	-13225	469	13408	8232	13408	8232	1.0

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	4495	--	17195	19915	17195	10.05	2.500	3.8
Z	(3+4)-II-2	--	--	11953	--	18069	34667	18069	10.05	2.500	1.5

Pilastro : 30 [7 , 107]

Sez. R: By= 30.0 cm Bz=90.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	Sezione non verificata
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05	

$v_{max}=N/(fcd*A)=0.107 \leq 0.65$ [Comb. (3+4)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-34167	-46586	-3984	46745	17206	46745	17206	0.75
	Sezione non verificata : Sezione non verificata								
Testa	(3+4)-I-1(+)	-29641	-2846	-10639	45681	16695	45681	16695	1.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	12353	26079	--	--	26079	10.05	2.500	2.1
Z	(3+4)-II-2	--	--	19253	--	36331	64170	36331	10.05	2.500	1.9

Pilastro : 30 [107 , 207]

Sez. R: By= 30.0 cm Bz=90.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05
Sezione non verificata			

$v_{max}=N/(fcd*A)=0.067 \leq 0.65$ [Comb. (3+4)-I-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-21548	-5603	15584	43718	15773	43718	15773	1.0
Testa	(3+4)-I-1(+)	-19726	-4742	-15856	43264	15563	43264	15563	0.75
Sezione non verificata : Sezione non verificata									

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	15466	24713	--	--	24713	10.05	2.500	1.6
Z	(3+4)-II-1	--	--	9869	--	34937	64170	34937	10.05	2.500	3.5

Pilastro : 30 [207 , 307]

Sez. R: By= 30.0 cm Bz=90.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 10.05

$v_{max}=N/(fcd*A)=0.049 \leq 0.65$ [Comb. (3+4)-I-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-15695	-5291	5463	42246	15096	42246	15096	3.2
Testa	(3+4)-II-2(+)	-11468	-11274	161	41156	14603	41156	14603	4.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	7925	23923	--	--	23923	10.05	2.500	3.0
Z	(3+4)-II-1	--	--	5977	--	34052	64170	34052	10.05	2.500	5.7

Pilastro : 30 [307 , 407]

Sez. R: By= 30.0 cm Bz=50.0 cm L=170.0 cm Ln=170.0 cm

Criterio : CLS_Pilastri-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 0.00	Afz = 4.02

$v_{max}=N/(fcd*A)=0.063 \leq 0.65$ [Comb. (3+4)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(+)	-11160	5258	-29	14139	8872	14139	8872	3.2
Testa	(3+4)-I-1(+)	-10331	6775	-7912	14032	8776	14032	8776	1.0

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	6369	--	17953	19915	17953	10.05	2.500	2.8
Z	(3+4)-II-2	--	--	4835	--	18294	34667	18294	10.05	2.500	3.8

Pilastro : 31 [16 , 116]

Sez. R: By= 90.0 cm Bz=30.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 3.14	Afy = 2.01	Afz = 2.01
Testa	AfSpigolo = 3.14	Afy = 2.01	Afz = 2.01

$$v_{\max} = N / (f_{cd} \cdot A) = 0.104 \leq 0.65 \quad [\text{Comb. (3+4)-I-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-32676	-2603	-1252	13477	44447	13477	44447	6.2
Testa	2(+)	-46152	1069	2077	14902	48444	14902	48444	6.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	4353	--	36718	64170	36718	10.05	2.500	8.4
Z	(3+4)-II-1	--	--	1161	24063	--	--	24063	10.05	2.500	21

Pilastro : 31 [116 , 216]

Sez. R: By= 90.0 cm Bz=30.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 5.99	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 5.99	Afz = 0.00

$$v_{\max} = N / (f_{cd} \cdot A) = 0.06 \leq 0.65 \quad [\text{Comb. (3+4)-II-2(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-16812	-2462	1109	11536	34062	11536	34062	7.8
Testa	(3+4)-II-1(+)	-16204	4041	-601	11464	33885	11464	33885	4.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	3626	--	34533	64170	34533	10.05	2.500	9.5
Z	(3+4)-II-1	--	--	3040	21732	--	--	21732	10.05	2.500	7.1

Pilastro : 31 [216 , 316]

Sez. R: By= 90.0 cm Bz=30.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 5.99	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 5.99	Afz = 0.00

$$v_{\max} = N / (f_{cd} \cdot A) = 0.044 \leq 0.65 \quad [\text{Comb. (3+4)-II-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-14081	-5447	-3099	11214	33263	11214	33263	2.5
Testa	(3+4)-I-3(+)	-10820	908	4101	10827	32275	10827	32275	9.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-II-1	--	--	5603	--	33860	64170	33860	10.05	2.500	6.0

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
Z	(3+4)-II-1	--	--	6926	21364	--	--	21364	10.05	2.500	3.1

Pilastro : 31 [316 , 416]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 170.0 \text{ cm}$ $L_n = 170.0 \text{ cm}$

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Sezione non verificata			

$v_{\max} = N/(fcd \cdot A) = 0.065 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-8820	-1909	2204	8601	13834	8601	13834	4.3
Testa	(3+4)-II-2(+)	-10798	-8717	6575	8830	14092	8830	14092	0.75
Sezione non verificata : Sezione non verificata									

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	8131	--	18825	34667	18825	10.05	2.500	2.3
Z	(3+4)-II-1	--	--	9064	--	17653	19915	17653	10.05	2.500	1.9

Pilastro : 32 [13 , 113]

Sez. R: $B_y = 90.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 300.0 \text{ cm}$ $L_n = 300.0 \text{ cm}$

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 2.01	Afz = 2.01
Testa	AfSpigolo = 3.14	Afy = 2.01	Afz = 2.01

$v_{\max} = N/(fcd \cdot A) = 0.102 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(-)	-31725	2845	1314	13374	44145	13374	44145	6.0
Testa	2(+)	-44922	-1155	-2021	14774	48100	14774	48100	6.9

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	4728	--	36607	64170	36607	10.05	2.500	7.7
Z	(3+4)-II-2	--	--	1296	23935	--	--	23935	10.05	2.500	18

Pilastro : 32 [113 , 213]

Sez. R: $B_y = 90.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 270.0 \text{ cm}$ $L_n = 270.0 \text{ cm}$

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 5.99	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 5.99	Afz = 0.00

$v_{\max} = N/(fcd \cdot A) = 0.057 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-1(-)	-16414	1703	5595	11489	33946	11489	33946	6.1
Testa	(3+4)-II-2(+)	-17660	-4031	-1067	11635	34307	11635	34307	4.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	4303	--	34210	64170	34210	10.05	2.500	7.9
Z	(3+4)-II-2	--	--	3043	21929	--	--	21929	10.05	2.500	7.2

Pilastro : 32 [213 , 313]

Sez. R: By= 90.0 cm Bz=30.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 5.99	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 5.99	Afz = 0.00

$$v_{\max} = N / (f_{cd} \cdot A) = 0.04 \leq 0.65 \quad [\text{Comb. (3+4)-II-2(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-9911	-5767	578	10719	31979	10719	31979	2.1
Testa	(3+4)-I-1(+)	-10164	-779	-4934	10749	32061	10749	32061	8.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	6643	--	33309	64170	33309	10.05	2.500	5.0
Z	(3+4)-II-2	--	--	8815	21203	--	--	21203	10.05	2.500	2.4

Pilastro : 32 [313 , 413]

Sez. R: By= 50.0 cm Bz=30.0 cm L=170.0 cm Ln=170.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Sezione non verificata			

$$v_{\max} = N / (f_{cd} \cdot A) = 0.06 \leq 0.65 \quad [\text{Comb. (3+4)-I-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(+)	-7733	978	-2297	8475	13690	8475	13690	5.8
Testa	(3+4)-I-1(+)	-10056	-5019	-11051	8744	13996	8744	13996	0.75
Sezione non verificata : Sezione non verificata									

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	7719	--	18711	34667	18711	10.05	2.500	2.4
Z	(3+4)-II-2	--	--	7429	--	17542	19915	17542	10.05	2.500	2.4

Pilastro : 33 [12 , 112]

Sez. R: By= 90.0 cm Bz=30.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 3.14	Afy = 2.01	Afz = 2.01
Testa	AfSpigolo = 3.14	Afy = 2.01	Afz = 2.01

$$v_{\max} = N / (f_{cd} \cdot A) = 0.101 \leq 0.65 \quad [\text{Comb. (3+4)-I-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(-)	-29245	2639	1570	13105	43295	13105	43295	6.4
Testa	2(+)	-44775	-1087	2015	14758	48059	14758	48059	7.0

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	4813	--	36597	64170	36597	10.05	2.500	7.6
Z	(3+4)-II-2	--	--	1166	23600	--	--	23600	10.05	2.500	20

Pilastro : 33 [112 , 212]

Sez. R: By= 90.0 cm Bz=30.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 10.05	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 10.05	Afz = 2.01

$$v_{\max} = N / (f_{cd} \cdot A) = 0.057 \leq 0.65 \quad [\text{Comb. (3+4)-II-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-17837	1246	-5297	17071	49207	17071	49207	8.9
Testa	(3+4)-II-2(+)	-15803	-4021	1292	16842	48691	16842	48691	5.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	4015	--	34423	64170	34423	10.05	2.500	8.6
Z	(3+4)-II-2	--	--	3014	25012	--	--	25012	10.05	2.500	8.3

Pilastro : 33 [212 , 312]

Sez. R: By= 90.0 cm Bz=30.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Verificato**

Piede	AfSpigolo = 2.01	Afy = 5.99	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 5.99	Afz = 0.00

$$v_{\max} = N / (f_{cd} \cdot A) = 0.041 \leq 0.65 \quad [\text{Comb. (3+4)-I-1(+)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(-)	-10511	5722	-2791	10790	32174	10790	32174	2.1
Testa	(3+4)-I-3(+)	-10124	-510	4804	10744	32048	10744	32048	9.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	6052	--	33303	64170	33303	10.05	2.500	5.5
Z	(3+4)-II-2	--	--	7934	20882	--	--	20882	10.05	2.500	2.6

Pilastro : 33 [312 , 412]

Sez. R: By= 50.0 cm Bz=30.0 cm L=170.0 cm Ln=170.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00

$$v_{\max} = N / (f_{cd} \cdot A) = 0.061 \leq 0.65 \quad [\text{Comb. (3+4)-I-3(-)}]$$

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(-)	-8668	1665	1765	8584	13814	8584	13814	5.2
Testa	(3+4)-II-1(+)	-10031	8333	5755	8742	13993	8742	13993	0.75
Sezione non verificata : Sezione non verificata									

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-3	--	--	7888	--	18740	34667	18740	10.05	2.500	2.4
Z	(3+4)-II-2	--	--	8307	--	17632	19915	17632	10.05	2.500	2.1

Pilastro : 34 [17 , 117]

Sez. R: By= 90.0 cm Bz=30.0 cm L=300.0 cm Ln=300.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 3.14	Afy = 2.01	Afz = 2.01
Testa	AfSpigolo = 3.14	Afy = 2.01	Afz = 2.01

$v_{max}=N/(fcd \cdot A)=0.124 \leq 0.65$ [Comb. (3+4)-I-3(-)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-39659	-1819	-5274	14222	46582	14222	46582	5.8
Testa	2(+)	-52285	1158	-2353	15457	50094	15457	50094	6.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	4263	--	36293	64170	36293	10.05	2.500	8.5
Z	(3+4)-II-1	--	--	1265	23915	--	--	23915	10.05	2.500	19

Pilastr : 34 [117 , 217]

Sez. R: By= 90.0 cm Bz=30.0 cm L=270.0 cm Ln=270.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 5.99	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 5.99	Afz = 0.00

$v_{max}=N/(fcd \cdot A)=0.078 \leq 0.65$ [Comb. (3+4)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-I-3(-)	-24393	-1743	-4179	12417	36205	12417	36205	7.2
Testa	(3+4)-II-1(+)	-24159	4041	239	12390	36140	12390	36140	4.9

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	3830	--	34539	64170	34539	10.05	2.500	9.0
Z	(3+4)-II-1	--	--	3057	22806	--	--	22806	10.05	2.500	7.5

Pilastr : 34 [217 , 317]

Sez. R: By= 90.0 cm Bz=30.0 cm L=110.0 cm Ln=110.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 :**Verificato**

Piede	AfSpigolo = 2.01	Afy = 5.99	Afz = 0.00
Testa	AfSpigolo = 2.01	Afy = 5.99	Afz = 0.00

$v_{max}=N/(fcd \cdot A)=0.062 \leq 0.65$ [Comb. (3+4)-II-1(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-2(-)	-11421	6602	444	10899	32470	10899	32470	1.8
Testa	(3+4)-II-2(+)	-11173	-3419	1121	10869	32389	10869	32389	4.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	2469	--	33609	64170	33609	10.05	2.500	14
Z	(3+4)-II-1	--	--	12661	22159	--	--	22159	10.05	2.500	1.8

Pilastr : 34 [317 , 417]

Sez. R: By= 50.0 cm Bz=30.0 cm L=170.0 cm Ln=170.0 cm

Criterio : CLS_Pilastr-Esist - Verifica a presso-flessione deviata:rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5 : **Non verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00
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Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 0.00	Sezione non verificata
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$v_{max}=N/(fcd*A)=0.072 \leq 0.65$ [Comb. (3+4)-II-2(+)]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kg	kg*m	kg*m	kg*m	kg*m	kg*m	kg*m	
Piede	(3+4)-II-1(-)	-8807	-3992	764	8600	13833	8600	13833	2.5
Testa	(3+4)-II-1(+)	-8170	10622	-8322	8526	13748	8526	13748	0.50
	Sezione non verificata : Sezione non verificata								

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kg*m	kg*m	kg	kg	kg	kg	kg	cmq/m		
Y	(3+4)-I-1	--	--	8017	--	18827	34667	18827	10.05	2.500	2.3
Z	(3+4)-II-1	--	--	11117	--	17651	19915	17651	10.05	2.500	1.6

Verifica delle travi

Scenario di calcolo : **Set_NT_SLV_SLD_A2_(STR/GEO)_2018**

Trave : 101 [0 , 104] Pilastrate [- , 4]

Sez. R: By= 45.0 cm Bz=30.0 cm L=125.0 cm Ln=125.0 cm

Criterio : CLS TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5

:: Non verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7243	2174	--	--	12.06	12.06	16125	16125	(3+4)-I-1	(5+6)-I-3	2.2
12.5	8276	1456	--	--	12.06	12.06	16125	16125	(3+4)-I-1	(5+6)-I-3	1.9
CAMP	17612	--	--	--	12.06	12.06	16125	16125	2	(5+6)-I-3	0.92

Sez. CAMP non verificata rispetto al criterio di verifica: Sezione non verificata

112.5	19570	--	--	--	12.06	12.06	16125	16125	2	(5+6)-I-3	0.82
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Sez. 112.5 non verificata rispetto al criterio di verifica: Sezione non verificata

FLN	21580	--	--	--	12.06	12.06	16125	16125	2	(5+6)-I-3	0.75
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Sez. FLN non verificata rispetto al criterio di verifica: Sezione non verificata

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.378	10.0	27.0	0.370	16125	16125	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
12.5	10.3	27.0	0.380	10.0	27.0	0.369	16125	16125	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
CAMP	7.4	27.0	0.272	--	--	--	16125	16125	2	(5+6)-I-3	Parz.	--
112.5	7.3	27.0	0.270	--	--	--	16125	16125	2	(5+6)-I-3	Parz.	--
FLN	6.7	27.0	0.250	--	--	--	16125	16125	2	(5+6)-I-3	Parz.	--

Verifica a taglio:cot(θ)=2.168

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	16301	--	16301	11513	11513	0	16125	125.0	6.70	0.71
Des							16125			

Sezione Insufficiente a Taglio

Trave : 101 [103 , 0] Pilastrate [3 , -]

Sez. R: By= 45.0 cm Bz=30.0 cm L=125.0 cm Ln=125.0 cm

Criterio : CLS TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5

:: Non verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
ILN	22951	--	--	--	12.06	12.06	16125	16125	2	(5+6)-I-1	0.70
Sez. ILN non verificata rispetto al criterio di verifica: Sezione non verificata											
12.5	20880	--	--	--	12.06	12.06	16125	16125	2	(5+6)-I-1	0.77
Sez. 12.5 non verificata rispetto al criterio di verifica: Sezione non verificata											
CAMP	18873	--	--	--	12.06	12.06	16125	16125	2	(5+6)-I-1	0.85
Sez. CAMP non verificata rispetto al criterio di verifica: Sezione non verificata											
112.5	8465	485	--	--	12.06	12.06	16125	16125	(3+4)-I-3	(5+6)-I-1	1.9
FLN	7396	1210	--	--	12.06	12.06	16125	16125	(3+4)-I-3	(5+6)-I-1	2.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	6.5	27.0	0.240	--	--	--	16125	16125	2	(5+6)-I-1	Parz.	--
12.5	7.3	27.0	0.269	--	--	--	16125	16125	2	(5+6)-I-1	Parz.	--
CAMP	7.3	27.0	0.270	--	--	--	16125	16125	2	(5+6)-I-1	Parz.	--
112.5	10.3	27.0	0.381	9.9	27.0	0.367	16125	16125	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
FLN	10.2	27.0	0.379	9.9	27.0	0.368	16125	16125	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.068$

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	16797	--	16797	16474	16474	0	16125	125.0	10.05	0.980
Des							16125			

Sezione Insufficiente a Taglio

Trave : 101 [101 , 0] Pilastrate [1 , -]

Sez. R: $B_y = 45.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 125.0 \text{ cm}$ $L_n = 125.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: **Non verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	21608	--	--	--	12.06	12.06	16125	16125	2	(5+6)-I-1	0.75
Sez. ILN non verificata rispetto al criterio di verifica: Sezione non verificata											
12.5	19607	--	--	--	12.06	12.06	16125	16125	2	(5+6)-I-1	0.82
Sez. 12.5 non verificata rispetto al criterio di verifica: Sezione non verificata											
CAMP	17658	--	--	--	12.06	12.06	16125	16125	2	(5+6)-I-1	0.91
Sez. CAMP non verificata rispetto al criterio di verifica: Sezione non verificata											
112.5	8227	1395	--	--	12.06	12.06	16125	16125	(3+4)-I-3	(5+6)-I-1	2.0
FLN	7168	2090	--	--	12.06	12.06	16125	16125	(3+4)-I-3	(5+6)-I-1	2.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	6.7	27.0	0.250	--	--	--	16125	16125	2	(5+6)-I-1	Parz.	--
12.5	7.3	27.0	0.270	--	--	--	16125	16125	2	(5+6)-I-1	Parz.	--
CAMP	7.3	27.0	0.272	--	--	--	16125	16125	2	(5+6)-I-1	Parz.	--
112.5	10.3	27.0	0.380	9.9	27.0	0.368	16125	16125	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
FLN	10.2	27.0	0.378	10.0	27.0	0.370	16125	16125	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.187$

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	16209	--	16209	17421	16209	0	16125	125.0	10.05	1.0
Des							16125			

Trave : 101 [0 , 0] Pilastrate [- , -]

Sez. R: $B_y = 45.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 585.0 \text{ cm}$ $L_n = 585.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7168	2090	--	--	12.06	12.06	16125	16125	(3+4)-I-3	(5+6)-I-1	2.2
58.5	2596	4749	--	--	12.06	12.06	16125	16125	(5+6)-I-3	(3+4)-I-1	3.4
CAMP	--	12330	--	--	12.06	12.06	16125	16125	(5+6)-II-1	2	1.3
526.5	2679	3833	--	--	12.06	12.06	16125	16125	(5+6)-I-1	(3+4)-I-3	4.2
FLN	7432	1111	--	--	12.06	12.06	16125	16125	(3+4)-I-1	(5+6)-I-3	2.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.378	10.0	27.0	0.370	16125	16125	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
58.5	10.0	27.0	0.370	10.1	27.0	0.374	16125	16125	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
CAMP	--	--	--	8.5	27.0	0.314	16125	16125	(5+6)-II-1	2	--	Parz.
526.5	10.0	27.0	0.370	10.1	27.0	0.372	16125	16125	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
FLN	10.2	27.0	0.379	9.9	27.0	0.368	16125	16125	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	11826	--	14779	13277	13277	0	16125	585.0	6.70	1.1
Des							16125			

Trave : 101 [0 , 0] Pilastrate [- , -]

Sez. R: $B_y = 45.0$ cm $B_z = 30.0$ cm $L = 585.0$ cm $L_n = 585.0$ cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7396	1210	--	--	12.06	12.06	16125	16125	(3+4)-I-3	(5+6)-I-1	2.2
58.5	2674	3887	--	--	12.06	12.06	16125	16125	(5+6)-I-3	(3+4)-I-1	4.1
CAMP	--	12171	--	--	12.06	12.06	16125	16125	(5+6)-II-1	2	1.3
526.5	2687	4820	--	--	12.06	12.06	16125	16125	(5+6)-I-1	(3+4)-I-3	3.3
FLN	7243	2174	--	--	12.06	12.06	16125	16125	(3+4)-I-1	(5+6)-I-3	2.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.379	9.9	27.0	0.368	16125	16125	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
58.5	10.0	27.0	0.370	10.1	27.0	0.372	16125	16125	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
CAMP	--	--	--	8.6	27.0	0.318	16125	16125	(5+6)-II-1	2	--	Parz.
526.5	10.0	27.0	0.370	10.1	27.0	0.374	16125	16125	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
FLN	10.2	27.0	0.378	10.0	27.0	0.370	16125	16125	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	11692	--	14779	13277	13277	0	16125	585.0	6.70	1.1
Des							16125			

Trave : 101 [0 , 102] Pilastrate [- , 2]

Sez. R: $B_y = 45.0$ cm $B_z = 30.0$ cm $L = 125.0$ cm $L_n = 125.0$ cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$

::Non verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
ILN	7432	1111	--	--	12.06	12.06	16125	16125	(3+4)-I-1	(5+6)-I-3	2.2
12.5	8507	376	--	--	12.06	12.06	16125	16125	(3+4)-I-1	(5+6)-I-3	1.9
CAMP	19132	--	--	--	12.06	12.06	16125	16125	2	(5+6)-I-3	0.84

Sez. CAMP non verificata rispetto al criterio di verifica: Sezione non verificata

112.5	21157	--	--	--	12.06	12.06	16125	16125	2	(5+6)-I-3	0.76
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Sez. 112.5 non verificata rispetto al criterio di verifica: Sezione non verificata

FLN	23247	--	--	--	12.06	12.06	16125	16125	2	(5+6)-I-3	0.69
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Sez. FLN non verificata rispetto al criterio di verifica: Sezione non verificata

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.379	9.9	27.0	0.368	16125	16125	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
12.5	10.3	27.0	0.381	9.9	27.0	0.367	16125	16125	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
CAMP	7.3	27.0	0.270	--	--	--	16125	16125	2	(5+6)-I-3	Parz.	--
112.5	7.3	27.0	0.269	--	--	--	16125	16125	2	(5+6)-I-3	Parz.	--
FLN	6.4	27.0	0.239	--	--	--	16125	16125	2	(5+6)-I-3	Parz.	--

Verifica a taglio: $\cot(\theta) = 2.038$

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	16951	--	16951	10821	10821	0	16125	125.0	6.70	0.64
Des							16125			

Sezione Insufficiente a Taglio

Trave : 101 [102 , 103] Pilastrate [2 , 3]

Sez. R: $B_y = 45.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 330.0 \text{ cm}$ $L_n = 330.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	15946	9575	--	--	12.06	12.06	16125	16125	(3+4)-I-3	(5+6)-I-1	1.0
33.0	12107	8222	--	--	12.06	12.06	16125	16125	(3+4)-I-3	(5+6)-I-1	1.3
CAMP	8652	--	--	--	12.06	12.06	16125	16125	(3+4)-I-1	1	1.9
297.0	12217	8122	--	--	12.06	12.06	16125	16125	(3+4)-I-1	(5+6)-I-3	1.3
FLN	16082	9448	--	--	12.06	12.06	16125	16125	(3+4)-I-1	(5+6)-I-3	1.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	7.1	27.0	0.263	10.3	27.0	0.383	16125	16125	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
33.0	8.6	27.0	0.320	10.3	27.0	0.380	16125	16125	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.381	--	--	--	16125	16125	(3+4)-I-1	1	Parz.	--
297.0	8.6	27.0	0.317	10.3	27.0	0.380	16125	16125	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	7.1	27.0	0.262	10.3	27.0	0.383	16125	16125	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	14695	--	14779	19915	14779	0	16125	330.0	10.05	1.0
Des							16125			

Trave : 102 [131 , 117] Pilastrate [22 , 34]

Sez. R: $B_y = 60.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 480.1 \text{ cm}$ $L_n = 480.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7959	--	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	3.0

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
48.0	4455	976	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	5.4
CAMP	--	4878	--	--	18.10	18.10	24144	24144	(5+6)-II-2	2	4.9
432.0	5017	945	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	4.8
FLN	8610	--	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	2.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.386	--	--	--	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	--
48.0	10.3	27.0	0.382	10.2	27.0	0.378	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	--	--	--	10.3	27.0	0.382	24144	24144	(5+6)-II-2	2	--	Parz.
432.0	10.3	27.0	0.383	10.2	27.0	0.378	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.4	27.0	0.387	--	--	--	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	--

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10891	--	19705	19915	19705	0	24144	480.0	10.05	1.8
Des							24144			

Trave : 102 [115 , 116] Pilastrate [17 , 31]

Sez. R: By= 60.0 cm Bz=30.0 cm L=395.1 cm Ln=395.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	9074	5463	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	2.7
39.5	6192	5516	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	3.9
CAMP	3892	5459	--	--	18.10	18.10	24144	24144	(5+6)-I-3	(3+4)-I-1	4.4
355.5	6584	2308	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	3.7
FLN	10021	1815	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	2.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.5	27.0	0.387	10.3	27.0	0.383	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
39.5	10.4	27.0	0.384	10.3	27.0	0.383	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.381	10.3	27.0	0.383	24144	24144	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
355.5	10.4	27.0	0.384	10.3	27.0	0.380	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.5	27.0	0.389	10.2	27.0	0.379	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10308	--	19705	19915	19705	0	24144	395.0	10.05	1.9
Des							24144			

Trave : 102 [117 , 118] Pilastrate [34 , 12]

Sez. R: By= 60.0 cm Bz=30.0 cm L=375.1 cm Ln=375.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	10016	1718	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	2.4
37.5	6720	2141	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	3.6
CAMP	3689	5396	--	--	18.10	18.10	24144	24144	(5+6)-I-1	(3+4)-I-3	4.5
337.5	5800	5585	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	4.2

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
FLN	8453	5684	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	2.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.5	27.0	0.389	10.2	27.0	0.379	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
37.5	10.4	27.0	0.385	10.2	27.0	0.379	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.381	10.3	27.0	0.383	24144	24144	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
337.5	10.4	27.0	0.384	10.3	27.0	0.383	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.4	27.0	0.387	10.4	27.0	0.383	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10407	--	19705	19915	19705	0	24144	375.0	10.05	1.9
Des							24144			

Trave : 102 [116 , 134] Pilastrate [31 , 21]

Sez. R: $B_y = 60.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 460.1 \text{ cm}$ $L_n = 460.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	8282	--	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	2.9
46.0	4904	1179	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	4.9
CAMP	--	4490	--	--	18.10	18.10	24144	24144	(5+6)-II-1	2	5.4
414.0	4397	1186	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	5.5
FLN	7701	--	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	3.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.386	--	--	--	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	--
46.0	10.3	27.0	0.383	10.2	27.0	0.378	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	--	--	--	10.3	27.0	0.382	24144	24144	(5+6)-II-1	2	--	Parz.
414.0	10.3	27.0	0.382	10.2	27.0	0.378	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.4	27.0	0.386	--	--	--	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	--

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10450	--	19705	19915	19705	0	24144	460.0	10.05	1.9
Des							24144			

Trave : 102 [134 , 131] Pilastrate [21 , 22]

Sez. R: $B_y = 60.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 310.0 \text{ cm}$ $L_n = 310.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7381	2176	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	3.3
31.0	5315	2203	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	4.5
CAMP	3814	411	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(3+4)-II-1	6.3
279.0	5697	1976	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	4.2
FLN	7848	1881	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	3.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.385	10.2	27.0	0.380	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
31.0	10.3	27.0	0.383	10.2	27.0	0.380	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.381	10.2	27.0	0.378	24144	24144	(3+4)-I-1	(3+4)-II-1	Parz.	Parz.
279.0	10.4	27.0	0.383	10.2	27.0	0.379	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.4	27.0	0.386	10.2	27.0	0.379	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8342	--	19705	19915	19705	0	24144	310.0	10.05	2.4
Des							24144			

Trave : 103 [112 , 133] Pilastrate [33 , 19]

Sez. R: By= 60.0 cm Bz=30.0 cm L=460.1 cm Ln=460.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	8556	230	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	2.8
46.0	5171	1563	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	4.7
CAMP	--	4389	--	--	18.10	18.10	24144	24144	(5+6)-II-2	2	5.5
414.0	4686	1506	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	5.2
FLN	7998	205	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	3.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.387	10.2	27.0	0.377	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
46.0	10.3	27.0	0.383	10.2	27.0	0.379	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	--	--	--	10.3	27.0	0.382	24144	24144	(5+6)-II-2	2	--	Parz.
414.0	10.3	27.0	0.382	10.2	27.0	0.379	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.4	27.0	0.386	10.2	27.0	0.377	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10177	--	19705	19915	19705	0	24144	460.0	10.05	1.9
Des							24144			

Trave : 103 [133 , 132] Pilastrate [19 , 20]

Sez. R: By= 60.0 cm Bz=30.0 cm L=310.0 cm Ln=310.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7769	2705	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	3.1
31.0	5657	2610	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	4.3
CAMP	4063	--	--	--	18.10	18.10	24144	24144	(3+4)-I-1	1	5.9
279.0	6000	2355	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	4.0
FLN	8193	2383	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	2.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.386	10.3	27.0	0.380	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
31.0	10.4	27.0	0.383	10.3	27.0	0.380	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	10.3	27.0	0.382	--	--	--	24144	24144	(3+4)-I-1	1	Parz.	--
279.0	10.4	27.0	0.384	10.3	27.0	0.380	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.4	27.0	0.386	10.3	27.0	0.380	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8561	--	19705	19915	19705	0	24144	310.0	10.05	2.3
Des							24144			

Trave : 103 [132 , 113] Pilastrate [20 , 32]

Sez. R: By= 60.0 cm Bz=30.0 cm L=479.6 cm Ln=479.5 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	8361	--	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	2.9
48.0	4821	1343	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	5.0
CAMP	--	4803	--	--	18.10	18.10	24144	24144	(5+6)-II-2	2	5.0
431.6	5356	1386	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	4.5
FLN	8996	--	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	2.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.387	--	--	--	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	--
48.0	10.3	27.0	0.382	10.2	27.0	0.379	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	--	--	--	10.3	27.0	0.382	24144	24144	(5+6)-II-2	2	--	Parz.
431.6	10.3	27.0	0.383	10.2	27.0	0.379	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.5	27.0	0.387	--	--	--	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	--

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10744	--	19705	19915	19705	0	24144	479.5	10.05	1.8
Des							24144			

Trave : 103 [113 , 114] Pilastrate [32 , 11]

Sez. R: By= 60.0 cm Bz=30.0 cm L=375.6 cm Ln=375.5 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	10777	2323	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	2.2
37.5	7312	2567	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	3.3
CAMP	4285	6234	--	--	18.10	18.10	24144	24144	(5+6)-I-1	(3+4)-I-3	3.9
337.9	6482	6648	--	--	18.10	18.10	24144	24144	(5+6)-I-1	(3+4)-I-3	3.6
FLN	9221	6993	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	2.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.5	27.0	0.390	10.3	27.0	0.380	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
37.5	10.4	27.0	0.385	10.3	27.0	0.380	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.382	10.4	27.0	0.384	24144	24144	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
337.9	10.4	27.0	0.384	10.4	27.0	0.385	24144	24144	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
FLN	10.5	27.0	0.388	10.4	27.0	0.385	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10990	--	19705	19915	19705	0	24144	375.5	10.05	1.8
Des							24144			

Trave : 103 [111 , 112] Pilastrate [18 , 33]

Sez. R: By= 60.0 cm Bz=30.0 cm L=395.1 cm Ln=395.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	9924	6292	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	2.4
39.5	6889	6196	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	3.5
CAMP	4442	5989	--	--	18.10	18.10	24144	24144	(5+6)-I-3	(3+4)-I-1	4.0
355.5	7015	2811	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	3.4
FLN	10563	2495	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	2.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.5	27.0	0.389	10.4	27.0	0.384	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
39.5	10.4	27.0	0.385	10.4	27.0	0.384	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.382	10.4	27.0	0.384	24144	24144	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
355.5	10.4	27.0	0.385	10.3	27.0	0.380	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.5	27.0	0.389	10.3	27.0	0.380	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10696	--	19705	19915	19705	0	24144	395.0	10.05	1.8
Des							24144			

Trave : 104 [122 , 123] Pilastrate [28 , 29]

Sez. R: By= 80.0 cm Bz=30.0 cm L=480.0 cm Ln=480.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	12386	2731	--	--	22.12	22.12	29548	29548	(3+4)-I-3	(5+6)-I-1	2.4
48.0	7669	3899	--	--	22.12	22.12	29548	29548	(3+4)-I-3	(5+6)-I-1	3.9
CAMP	5104	5184	--	--	22.12	22.12	29548	29548	(3+4)-I-1	2	5.7
432.0	9217	3407	--	--	22.12	22.12	29548	29548	(3+4)-I-1	(5+6)-I-3	3.2
FLN	14011	2159	--	--	22.12	22.12	29548	29548	(3+4)-I-1	(5+6)-I-3	2.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.380	10.0	27.0	0.371	29548	29548	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
48.0	10.1	27.0	0.376	10.1	27.0	0.372	29548	29548	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.1	27.0	0.374	10.1	27.0	0.374	29548	29548	(3+4)-I-1	2	Parz.	Parz.
432.0	10.2	27.0	0.377	10.0	27.0	0.372	29548	29548	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.3	27.0	0.382	10.0	27.0	0.371	29548	29548	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	12272	--	26274	19915	19915	0	29548	480.0	10.05	1.6
Des							29548			

Trave : 104 | 119 , 120 | Pilastrate [16 , 26]

Sez. R: By= 80.0 cm Bz=30.0 cm L=510.2 cm Ln=511.2 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²], fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

:: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	12982	2591	--	--	22.12	22.12	29548	29548	(3+4)-I-3	(5+6)-I-1	2.3
51.1	7442	4404	--	--	22.12	22.12	29548	29548	(3+4)-I-3	(5+6)-I-1	4.0
CAMP	--	8743	--	--	22.12	22.12	29548	29548	(5+6)-II-2	2	3.4
460.1	10032	2248	--	--	22.12	22.12	29548	29548	(3+4)-I-1	(5+6)-I-3	2.9
FLN	16731	--	--	--	22.12	22.12	29548	29548	(3+4)-I-1	(5+6)-I-3	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.381	10.0	27.0	0.371	29548	29548	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
51.1	10.1	27.0	0.376	10.1	27.0	0.373	29548	29548	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	--	--	--	10.2	27.0	0.377	29548	29548	(5+6)-II-2	2	--	Parz.
460.1	10.2	27.0	0.378	10.0	27.0	0.371	29548	29548	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.4	27.0	0.385	--	--	--	29548	29548	(3+4)-I-1	(5+6)-I-3	Parz.	--

Verifica a taglio: cot(θ) = 2.500

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	18503	--	26274	19915	19915	0	29548	511.2	10.05	1.1
Des							29548			

Trave : 104 | 123 , 155 | Pilastrate [29 , -]

Sez. R: By= 60.0 cm Bz=30.0 cm L=375.0 cm Ln=375.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²], fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

:: **Non verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	12050	87	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	2.0
37.5	8820	1126	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	2.7
CAMP	5973	2595	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(3+4)-I-1	4.0
337.5	1133	3822	--	--	18.10	18.10	24144	24144	(5+6)-I-1	(3+4)-I-3	6.3
FLN	2619	3886	--	--	18.10	18.10	24144	24144	(5+6)-I-1	(3+4)-I-3	6.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.6	27.0	0.391	10.2	27.0	0.377	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
37.5	10.5	27.0	0.387	10.2	27.0	0.378	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.4	27.0	0.384	10.3	27.0	0.380	24144	24144	(3+4)-I-3	(3+4)-I-1	Parz.	Parz.
337.5	10.2	27.0	0.378	10.3	27.0	0.381	24144	24144	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
FLN	10.3	27.0	0.380	10.3	27.0	0.381	24144	24144	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.

Verifica a taglio: cot(θ) = 2.500

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10934	--	19705	9957	9957	0	24144	375.0	5.03	0.91
Des							24144			

Sezione Insufficiente a Taglio

Trave : 104 [120 , 121] Pilastrate [26 , 27]

Sez. R: By= 60.0 cm Bz=30.0 cm L=345.0 cm Ln=345.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

:: **Non verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	12676	3563	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	1.9
34.5	8840	3915	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	2.7
CAMP	5493	2855	--	--	18.10	18.10	24144	24144	(3+4)-I-3	2	4.4
310.5	7137	4912	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	3.4
FLN	10514	4930	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	2.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.6	27.0	0.392	10.3	27.0	0.381	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
34.5	10.5	27.0	0.387	10.3	27.0	0.381	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.383	10.3	27.0	0.380	24144	24144	(3+4)-I-3	2	Parz.	Parz.
310.5	10.4	27.0	0.385	10.3	27.0	0.383	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.5	27.0	0.389	10.3	27.0	0.383	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =(3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	13284	--	19705	9957	9957	0	24144	345.0	5.03	0.75
Des							24144			

Sezione Insufficiente a Taglio

Trave : 104 [121 , 122] Pilastrate [27 , 28]

Sez. R: By= 80.0 cm Bz=30.0 cm L=310.0 cm Ln=310.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

:: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	11808	9347	--	--	22.12	22.12	29548	29548	(3+4)-I-3	(5+6)-I-1	2.5
31.0	8989	7871	--	--	22.12	22.12	29548	29548	(3+4)-I-3	(5+6)-I-1	3.3
CAMP	7208	--	--	--	22.12	22.12	29548	29548	(3+4)-I-1	1	4.1
279.0	10130	6853	--	--	22.12	22.12	29548	29548	(3+4)-I-1	(5+6)-I-3	2.9
FLN	13247	8089	--	--	22.12	22.12	29548	29548	(3+4)-I-1	(5+6)-I-3	2.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.380	10.2	27.0	0.377	29548	29548	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
31.0	10.2	27.0	0.377	10.2	27.0	0.376	29548	29548	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.1	27.0	0.375	--	--	--	29548	29548	(3+4)-I-1	1	Parz.	--
279.0	10.2	27.0	0.378	10.1	27.0	0.375	29548	29548	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.3	27.0	0.381	10.2	27.0	0.376	29548	29548	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	12615	--	26274	19915	19915	0	29548	310.0	10.05	1.6
Des							29548			

Trave : 105 [125 , 124] Pilastrate [14 , 15]

Sez. R: By= 45.0 cm Bz=30.0 cm L=450.0 cm Ln=450.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7427	2745	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	2.2
45.0	5110	3033	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	3.2
CAMP	3063	3056	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	5.3
405.0	4788	2938	--	--	12.06	12.06	16125	16125	(5+6)-II-1	(3+4)-II-2	3.4
FLN	7002	2685	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	2.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.379	10.0	27.0	0.371	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
45.0	10.1	27.0	0.375	10.0	27.0	0.371	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.0	27.0	0.371	10.0	27.0	0.371	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
405.0	10.1	27.0	0.374	10.0	27.0	0.371	16125	16125	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	10.2	27.0	0.378	10.0	27.0	0.370	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =(3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6168	--	14779	19915	14779	0	16125	450.0	10.05	2.4
Des							16125			

Trave : 105 [124 , 119] Pilastrate [15 , 16]

Sez. R: By= 45.0 cm Bz=30.0 cm L=470.0 cm Ln=470.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	8682	2079	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	1.9
47.0	5760	2726	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	2.8
CAMP	3565	2548	--	--	12.06	12.06	16125	16125	(3+4)-II-1	2	4.5
423.0	6139	2592	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	2.6
FLN	9099	1896	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.381	10.0	27.0	0.370	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
47.0	10.1	27.0	0.376	10.0	27.0	0.371	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.0	27.0	0.372	10.0	27.0	0.370	16125	16125	(3+4)-II-1	2	Parz.	Parz.
423.0	10.2	27.0	0.376	10.0	27.0	0.370	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.382	10.0	27.0	0.369	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =(3+4)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7413	--	14779	19915	14779	0	16125	470.0	10.05	2.0
Des							16125			

Trave : 105 [119 , 115] Pilastrate [16 , 17]

Sez. R: By= 45.0 cm Bz=30.0 cm L=450.0 cm Ln=450.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	10097	1649	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	1.6
45.0	6484	2750	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	2.5
CAMP	3395	3925	--	--	12.06	12.06	16125	16125	(3+4)-II-2	2	4.1
405.0	6503	2312	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	2.5
FLN	10190	1147	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.384	10.0	27.0	0.369	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
45.0	10.2	27.0	0.377	10.0	27.0	0.371	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.0	27.0	0.372	10.1	27.0	0.373	16125	16125	(3+4)-II-2	2	Parz.	Parz.
405.0	10.2	27.0	0.377	10.0	27.0	0.370	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.4	27.0	0.384	9.9	27.0	0.368	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	9871	--	14779	19915	14779	0	16125	450.0	10.05	1.5
Des							16125			

Trave : 105 [115 , 111] Pilastrate [17 , 18]

Sez. R: $B_y = 45.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 330.0 \text{ cm}$ $L_n = 330.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	9832	4526	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	1.6
33.0	7066	4318	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	2.3
CAMP	4562	1682	--	--	12.06	12.06	16125	16125	(3+4)-II-2	2	3.5
297.0	6973	4417	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	2.3
FLN	9712	4646	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	1.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.383	10.1	27.0	0.374	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
33.0	10.2	27.0	0.378	10.1	27.0	0.373	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.1	27.0	0.374	10.0	27.0	0.369	16125	16125	(3+4)-II-2	2	Parz.	Parz.
297.0	10.2	27.0	0.378	10.1	27.0	0.373	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.383	10.1	27.0	0.374	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10018	--	14779	19915	14779	0	16125	330.0	10.05	1.5
Des							16125			

Trave : 105 [111 , 105] Pilastrate [18 , 9]

Sez. R: $B_y = 45.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 440.0 \text{ cm}$ $L_n = 440.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: **Verificato**

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	10093	1264	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	1.6
44.0	6499	2341	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	2.5

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
CAMP	3374	3738	--	--	12.06	12.06	16125	16125	(3+4)-II-1	2	4.3
396.0	6366	2881	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	2.5
FLN	9817	1938	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.384	9.9	27.0	0.368	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
44.0	10.2	27.0	0.377	10.0	27.0	0.370	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.0	27.0	0.372	10.0	27.0	0.372	16125	16125	(3+4)-II-1	2	Parz.	Parz.
396.0	10.2	27.0	0.377	10.0	27.0	0.371	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.4	27.0	0.383	10.0	27.0	0.369	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	9713	--	14779	19915	14779	0	16125	440.0	10.05	1.5
Des							16125			

Trave : 105 [105 , 101] Pilastrate [9 , 1]

Sez. R: $B_y = 45.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 470.1 \text{ cm}$ $L_n = 470.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	11614	--	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	1.4
47.0	7519	1264	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	2.1
CAMP	--	4542	--	--	12.06	12.06	16125	16125	(5+6)-I-3	2	3.5
423.0	5014	3263	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	3.2
FLN	8562	2112	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	1.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.1	27.0	0.337	--	--	--	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	--
47.0	10.2	27.0	0.379	9.9	27.0	0.368	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	--	--	--	10.1	27.0	0.374	16125	16125	(5+6)-I-3	2	--	Parz.
423.0	10.1	27.0	0.374	10.0	27.0	0.371	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.381	10.0	27.0	0.370	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10647	--	14779	19915	14779	0	16125	470.0	10.05	1.4
Des							16125			

Trave : 106 [114 , 110] Pilastrate [11 , 10]

Sez. R: $B_y = 45.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 440.0 \text{ cm}$ $L_n = 440.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	10368	1981	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	1.6
44.0	6718	2915	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	2.4
CAMP	3809	3786	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(3+4)-II-2	4.2
396.0	6949	3135	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	2.3
FLN	10545	2255	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.385	10.0	27.0	0.369	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
44.0	10.2	27.0	0.377	10.0	27.0	0.371	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.1	27.0	0.372	10.1	27.0	0.372	16125	16125	(3+4)-II-1	(3+4)-II-2	Parz.	Parz.
396.0	10.2	27.0	0.378	10.0	27.0	0.371	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.4	27.0	0.385	10.0	27.0	0.370	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	9703	--	14779	19915	14779	0	16125	440.0	10.05	1.5
Des							16125			

Trave : 106 [110 , 104] Pilastrate [10 , 4]

Sez. R: $B_y = 45.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 470.1 \text{ cm}$ $L_n = 470.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cm}^2\text{]}$, $f_{ym} = 4500 \text{ [kg/cm}^2\text{]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	11840	326	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	1.4
47.0	7699	1831	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	2.1
CAMP	--	4542	--	--	12.06	12.06	16125	16125	(5+6)-I-3	2	3.5
423.0	5582	3451	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	2.9
FLN	9275	2349	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	1.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	8.9	27.0	0.329	9.9	27.0	0.367	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
47.0	10.2	27.0	0.379	10.0	27.0	0.369	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	--	--	--	10.1	27.0	0.374	16125	16125	(5+6)-I-3	2	--	Parz.
423.0	10.1	27.0	0.375	10.0	27.0	0.372	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.382	10.0	27.0	0.370	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10554	--	14779	19915	14779	0	16125	470.0	10.05	1.4
Des							16125			

Trave : 106 [130 , 155] Pilastrate [13 , -]

Sez. R: $B_y = 45.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 135.0 \text{ cm}$ $L_n = 135.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cm}^2\text{]}$, $f_{ym} = 4500 \text{ [kg/cm}^2\text{]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Non verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	12781	--	--	--	12.06	12.06	16125	16125	(3+4)-I-1	(5+6)-I-3	1.3
13.5	11225	--	--	--	12.06	12.06	16125	16125	(3+4)-I-1	(5+6)-I-3	1.4
CAMP	9688	2649	--	--	12.06	12.06	16125	16125	(3+4)-I-1	(3+4)-II-1	1.7
121.5	893	3349	--	--	12.06	12.06	16125	16125	(5+6)-II-2	(3+4)-II-1	4.8
FLN	--	4036	--	--	12.06	12.06	16125	16125	(5+6)-II-2	(3+4)-II-1	4.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
ILN	8.2	27.0	0.302	--	--	--	16125	16125	(3+4)-I-1	(5+6)-I-3	Parz.	--
13.5	9.6	27.0	0.354	--	--	--	16125	16125	(3+4)-I-1	(5+6)-I-3	Parz.	--
CAMP	10.3	27.0	0.383	10.0	27.0	0.370	16125	16125	(3+4)-I-1	(3+4)-II-1	Parz.	Parz.
121.5	9.9	27.0	0.368	10.0	27.0	0.372	16125	16125	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
FLN	--	--	--	10.1	27.0	0.373	16125	16125	(5+6)-II-2	(3+4)-II-1	--	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	13153	--	14779	9957	9957	0	16125	135.0	5.03	0.76
Des							16125			

Sezione Insufficiente a Taglio

Trave : 106 [155 , 118] Pilastrate [- , 12]

Sez. R: $B_y = 45.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 465.0 \text{ cm}$ $L_n = 465.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3619	4062	--	--	12.06	12.06	16125	16125	(5+6)-II-2	(3+4)-II-1	4.0
46.5	1063	5071	--	--	12.06	12.06	16125	16125	(5+6)-II-2	(3+4)-II-1	3.2
CAMP	--	6777	--	--	12.06	12.06	16125	16125	(5+6)-II-2	2	2.4
418.5	8865	301	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	1.8
FLN	13360	--	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	1.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.0	27.0	0.372	10.1	27.0	0.373	16125	16125	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
46.5	9.9	27.0	0.368	10.1	27.0	0.374	16125	16125	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
CAMP	--	--	--	10.2	27.0	0.378	16125	16125	(5+6)-II-2	2	--	Parz.
418.5	10.3	27.0	0.382	9.9	27.0	0.367	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	7.9	27.0	0.291	--	--	--	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	--

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	13021	--	14779	19915	14779	0	16125	465.0	10.05	1.1
Des							16125			

Trave : 106 [118 , 114] Pilastrate [12 , 11]

Sez. R: $B_y = 45.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 330.0 \text{ cm}$ $L_n = 330.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	11140	4779	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	1.4
33.0	8144	4507	--	--	12.06	12.06	16125	16125	(3+4)-II-2	(5+6)-II-1	2.0
CAMP	5408	1483	--	--	12.06	12.06	16125	16125	(3+4)-II-2	2	3.0
297.0	7264	5154	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	2.2
FLN	10053	5600	--	--	12.06	12.06	16125	16125	(3+4)-II-1	(5+6)-II-2	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.7	27.0	0.359	10.1	27.0	0.374	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
33.0	10.3	27.0	0.380	10.1	27.0	0.374	16125	16125	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	10.1	27.0	0.375	10.0	27.0	0.369	16125	16125	(3+4)-II-2	2	Parz.	Parz.
297.0	10.2	27.0	0.378	10.1	27.0	0.375	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.4	27.0	0.384	10.1	27.0	0.375	16125	16125	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10859	--	14779	19915	14779	0	16125	330.0	10.05	1.4
Des							16125			

Trave : 107 [129 , 128] Pilastrate [8 , 5]

Sez. R: $B_y = 30.0 \text{ cm}$ $B_z = 50.0 \text{ cm}$ $L = 517.0 \text{ cm}$ $L_n = 516.4 \text{ cm}$

Criterio : CLS_TraviAlte_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	13759	3670	--	--	12.06	12.06	20046	20046	(3+4)-I-1	(5+6)-I-3	1.5
51.6	9028	4494	--	--	12.06	12.06	20046	20046	(3+4)-I-1	(5+6)-I-3	2.2
CAMP	5342	6600	--	--	12.06	12.06	20046	20046	(5+6)-I-3	(3+4)-I-1	3.0
464.7	9209	6332	--	--	12.06	12.06	20046	20046	(3+4)-I-3	(5+6)-I-1	2.2
FLN	13874	5572	--	--	12.06	12.06	20046	20046	(3+4)-I-3	(5+6)-I-1	1.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	16.6	47.0	0.352	16.2	47.0	0.344	20046	20046	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
51.6	16.4	47.0	0.348	16.2	47.0	0.345	20046	20046	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
CAMP	16.2	47.0	0.345	16.3	47.0	0.346	20046	20046	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
464.7	16.4	47.0	0.348	16.3	47.0	0.346	20046	20046	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
FLN	16.6	47.0	0.352	16.2	47.0	0.345	20046	20046	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10895	--	17151	34667	17151	0	20046	516.4	10.05	1.6
Des							20046			

Trave : 107 [130 , 129] Pilastrate [13 , 8]

Sez. R: $B_y = 30.0 \text{ cm}$ $B_z = 50.0 \text{ cm}$ $L = 395.2 \text{ cm}$ $L_n = 395.2 \text{ cm}$

Criterio : CLS_TraviAlte_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	8634	4524	--	--	12.06	12.06	20046	20046	(3+4)-I-1	(5+6)-I-3	2.3
39.5	5990	4333	--	--	12.06	12.06	20046	20046	(3+4)-I-1	(5+6)-I-3	3.3
CAMP	5102	3886	--	--	12.06	12.06	20046	20046	(3+4)-I-3	(5+6)-I-1	3.9
355.7	7767	4094	--	--	12.06	12.06	20046	20046	(3+4)-I-3	(5+6)-I-1	2.6
FLN	10778	3992	--	--	12.06	12.06	20046	20046	(3+4)-I-3	(5+6)-I-1	1.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	16.4	47.0	0.348	16.2	47.0	0.345	20046	20046	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
39.5	16.3	47.0	0.346	16.2	47.0	0.345	20046	20046	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
CAMP	16.2	47.0	0.345	16.2	47.0	0.344	20046	20046	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
355.7	16.3	47.0	0.347	16.2	47.0	0.344	20046	20046	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
FLN	16.4	47.0	0.350	16.2	47.0	0.344	20046	20046	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	9207	--	17151	34667	17151	0	20046	395.2	10.05	1.9
Des							20046			

Trave : 108 [126 , 125] Pilastrate [7 , 14]

Sez. R: By= 30.0 cm Bz=50.0 cm L=444.9 cm Ln=442.9 cm

Criterio : CLS_TraviAlte_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	10461	3163	--	--	12.06	12.06	20046	20046	(3+4)-I-1	(5+6)-I-3	1.9
44.3	7299	3512	--	--	12.06	12.06	20046	20046	(3+4)-I-1	(5+6)-I-3	2.7
CAMP	--	5487	--	--	12.06	12.06	20046	20046	(5+6)-II-2	(3+4)-I-1	3.7
398.7	5152	5679	--	--	12.06	12.06	20046	20046	(5+6)-I-3	(3+4)-I-1	3.5
FLN	8070	5561	--	--	12.06	12.06	20046	20046	(3+4)-I-3	(5+6)-I-1	2.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	16.4	47.0	0.349	16.2	47.0	0.344	20046	20046	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
44.3	16.3	47.0	0.347	16.2	47.0	0.344	20046	20046	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
CAMP	--	--	--	16.2	47.0	0.345	20046	20046	(5+6)-II-2	(3+4)-I-1	--	Parz.
398.7	16.2	47.0	0.345	16.2	47.0	0.346	20046	20046	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
FLN	16.3	47.0	0.347	16.2	47.0	0.345	20046	20046	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8453	--	17151	34667	17151	0	20046	442.9	10.05	2.0
Des							20046			

Trave : 108 [127 , 126] Pilastrate [6 , 7]

Sez. R: By= 30.0 cm Bz=50.0 cm L=450.0 cm Ln=448.4 cm

Criterio : CLS_TraviAlte_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	14963	5755	--	--	12.06	12.06	20046	20046	(3+4)-I-1	(5+6)-I-3	1.3
44.8	10193	6366	--	--	12.06	12.06	20046	20046	(3+4)-I-1	(5+6)-I-3	2.0
CAMP	6094	6442	--	--	12.06	12.06	20046	20046	(5+6)-I-1	(3+4)-I-3	3.1
403.6	9568	4471	--	--	12.06	12.06	20046	20046	(3+4)-I-3	(5+6)-I-1	2.1
FLN	14536	3693	--	--	12.06	12.06	20046	20046	(3+4)-I-3	(5+6)-I-1	1.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	16.6	47.0	0.353	16.2	47.0	0.346	20046	20046	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
44.8	16.4	47.0	0.349	16.3	47.0	0.346	20046	20046	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
CAMP	16.3	47.0	0.346	16.3	47.0	0.346	20046	20046	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
403.6	16.4	47.0	0.349	16.2	47.0	0.345	20046	20046	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
FLN	16.6	47.0	0.353	16.2	47.0	0.344	20046	20046	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	13073	--	17151	34667	17151	0	20046	448.4	10.05	1.3
Des							20046			

Trave : 109 [127 , 121] Pilastrate [6 , 27]

Sez. R: By= 30.0 cm Bz=50.0 cm L=598.6 cm Ln=598.7 cm

Criterio : CLS_TraviAlte_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	13767	5745	--	--	12.06	12.06	20046	20046	(3+4)-II-2	(5+6)-II-1	1.5
59.9	8777	6118	--	--	12.06	12.06	20046	20046	(3+4)-II-2	(5+6)-II-1	2.3
CAMP	8395	7547	--	--	12.06	12.06	20046	20046	(3+4)-II-1	(5+6)-II-2	2.4
538.8	13171	7379	--	--	12.06	12.06	20046	20046	(3+4)-II-1	(5+6)-II-2	1.5
FLN	18608	6605	--	--	12.06	12.06	20046	20046	(3+4)-II-1	(5+6)-II-2	1.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	16.6	47.0	0.352	16.2	47.0	0.346	20046	20046	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
59.9	16.4	47.0	0.348	16.3	47.0	0.346	20046	20046	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	16.3	47.0	0.348	16.3	47.0	0.347	20046	20046	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
538.8	16.5	47.0	0.352	16.3	47.0	0.347	20046	20046	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	16.8	47.0	0.357	16.3	47.0	0.346	20046	20046	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio:cot(θ)=2.500

Comb =(3+4)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10807	--	17151	34667	17151	0	20046	598.7	10.05	1.6
Des							20046			

Trave : 110 [128 , 122] Pilastrate [5 , 28]

Sez. R: By= 30.0 cm Bz=50.0 cm L=472.3 cm Ln=472.4 cm

Criterio : CLS_TraviAlte_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	12286	9455	--	--	12.06	12.06	20046	20046	(3+4)-II-2	(5+6)-II-1	1.6
47.2	8383	8229	--	--	12.06	12.06	20046	20046	(3+4)-II-2	(5+6)-II-1	2.4
CAMP	9737	9127	--	--	12.06	12.06	20046	20046	(5+6)-II-1	(3+4)-II-2	2.1
425.1	13899	10061	--	--	12.06	12.06	20046	20046	(3+4)-II-1	(5+6)-II-2	1.4
FLN	18512	10646	--	--	12.06	12.06	20046	20046	(3+4)-II-1	(5+6)-II-2	1.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	16.5	47.0	0.351	16.4	47.0	0.349	20046	20046	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
47.2	16.3	47.0	0.348	16.3	47.0	0.348	20046	20046	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	16.4	47.0	0.349	16.4	47.0	0.348	20046	20046	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
425.1	16.6	47.0	0.352	16.4	47.0	0.349	20046	20046	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	16.8	47.0	0.357	16.4	47.0	0.350	20046	20046	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio:cot(θ)=2.500

Comb =(3+4)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	11953	--	17151	34667	17151	0	20046	472.4	10.05	1.4
Des							20046			

Trave : 111 | 108 , 109 | Pilastrate [24 , 25]

Sez. R: By= 60.0 cm Bz=30.0 cm L=347.3 cm Ln=339.2 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5:: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	15104	10269	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	1.6
33.9	11059	9040	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	2.2
CAMP	8218	2161	--	--	18.10	18.10	24144	24144	(3+4)-I-1	2	2.9
305.3	12193	7921	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	2.0
FLN	16527	8902	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.7	27.0	0.396	10.5	27.0	0.389	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
33.9	10.5	27.0	0.390	10.5	27.0	0.387	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.4	27.0	0.386	10.2	27.0	0.379	24144	24144	(3+4)-I-1	2	Parz.	Parz.
305.3	10.6	27.0	0.391	10.4	27.0	0.386	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.1	27.0	0.375	10.5	27.0	0.387	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	15451	--	19705	19915	19705	0	24144	339.2	10.05	1.3
Des							24144			

Trave : 111 | 109 , 110 | Pilastrate [25 , 10]

Sez. R: By= 80.0 cm Bz=30.0 cm L=510.1 cm Ln=509.3 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5:: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	18643	3772	--	--	22.12	22.12	29548	29548	(3+4)-I-3	(5+6)-I-1	1.6
50.9	12220	5115	--	--	22.12	22.12	29548	29548	(3+4)-I-3	(5+6)-I-1	2.4
CAMP	--	8235	--	--	22.12	22.12	29548	29548	(5+6)-II-2	(3+4)-I-3	3.6
458.4	9563	7862	--	--	22.12	22.12	29548	29548	(3+4)-I-1	(5+6)-I-3	3.1
FLN	15217	7158	--	--	22.12	22.12	29548	29548	(3+4)-I-1	(5+6)-I-3	1.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.5	27.0	0.387	10.1	27.0	0.372	29548	29548	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
50.9	10.3	27.0	0.380	10.1	27.0	0.374	29548	29548	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	--	--	--	10.2	27.0	0.376	29548	29548	(5+6)-II-2	(3+4)-I-3	--	Parz.
458.4	10.2	27.0	0.378	10.2	27.0	0.376	29548	29548	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.4	27.0	0.383	10.1	27.0	0.375	29548	29548	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	14951	--	26274	19915	19915	0	29548	509.3	10.05	1.3
Des							29548			

Trave : 111 | 105 , 106 | Pilastrate [9 , 23]

Sez. R: By= 80.0 cm Bz=30.0 cm L=510.1 cm Ln=510.7 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$
::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	15470	7119	--	--	22.12	22.12	29548	29548	(3+4)-I-3	(5+6)-I-1	1.9
51.1	9766	7819	--	--	22.12	22.12	29548	29548	(3+4)-I-3	(5+6)-I-1	3.0
CAMP	--	8190	--	--	22.12	22.12	29548	29548	(5+6)-II-1	(3+4)-I-1	3.6
459.6	12267	5310	--	--	22.12	22.12	29548	29548	(3+4)-I-1	(5+6)-I-3	2.4
FLN	18707	4000	--	--	22.12	22.12	29548	29548	(3+4)-I-1	(5+6)-I-3	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.384	10.1	27.0	0.375	29548	29548	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
51.1	10.2	27.0	0.378	10.2	27.0	0.376	29548	29548	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	--	--	--	10.2	27.0	0.376	29548	29548	(5+6)-II-1	(3+4)-I-1	--	Parz.
459.6	10.3	27.0	0.380	10.1	27.0	0.374	29548	29548	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.5	27.0	0.387	10.1	27.0	0.373	29548	29548	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$
Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	14927	--	26274	19915	19915	0	29548	510.7	10.05	1.3
Des							29548			

Trave : 111 [106 , 107] Pilastrate [23 , 30]

Sez. R: $B_y = 60.0$ cm $B_z = 30.0$ cm $L = 347.3$ cm $L_n = 338.7$ cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$
::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	15850	8582	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	1.5
33.9	11632	7677	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	2.1
CAMP	7797	2166	--	--	18.10	18.10	24144	24144	(3+4)-I-3	2	3.1
304.8	10794	8552	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	2.2
FLN	14784	9639	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.7	27.0	0.397	10.4	27.0	0.387	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
33.9	10.5	27.0	0.391	10.4	27.0	0.386	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.4	27.0	0.386	10.2	27.0	0.379	24144	24144	(3+4)-I-3	2	Parz.	Parz.
304.8	10.5	27.0	0.390	10.4	27.0	0.387	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.7	27.0	0.395	10.5	27.0	0.388	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$
Comb = (3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	15325	--	19705	19915	19705	0	24144	338.7	10.05	1.3
Des							24144			

Trave : 111 [107 , 108] Pilastrate [30 , 24]

Sez. R: $B_y = 60.0$ cm $B_z = 30.0$ cm $L = 310.0$ cm $L_n = 310.0$ cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$
::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
ILN	15404	10851	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	1.6
31.0	11443	9390	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	2.1
CAMP	7854	2086	--	--	18.10	18.10	24144	24144	(3+4)-I-1	2	3.1
279.0	11541	9169	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	2.1
FLN	15543	10592	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.7	27.0	0.396	10.5	27.0	0.390	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
31.0	10.5	27.0	0.390	10.5	27.0	0.388	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.4	27.0	0.386	10.2	27.0	0.379	24144	24144	(3+4)-I-1	2	Parz.	Parz.
279.0	10.5	27.0	0.391	10.5	27.0	0.388	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.7	27.0	0.396	10.5	27.0	0.389	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	16176	--	19705	19915	19705	0	24144	310.0	10.05	1.2
Des							24144			

Trave : 112 [126 , 124] Pilastrate [7 , 15]

Sez. R: By= 80.0 cm Bz=30.0 cm L=518.2 cm Ln=510.3 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	9331	--	--	--	22.12	22.12	29548	29548	2	(5+6)-I-3	3.2
51.0	5030	833	--	--	22.12	22.12	29548	29548	(3+4)-II-2	(5+6)-II-1	5.9
CAMP	--	6985	--	--	22.12	22.12	29548	29548	(5+6)-I-3	2	4.2
459.2	4683	2016	--	--	22.12	22.12	29548	29548	(3+4)-I-3	(5+6)-I-1	6.3
FLN	8889	--	--	--	22.12	22.12	29548	29548	(3+4)-I-3	(5+6)-I-1	3.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.377	--	--	--	29548	29548	2	(5+6)-I-3	Parz.	--
51.0	10.1	27.0	0.373	10.0	27.0	0.370	29548	29548	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	--	--	--	10.1	27.0	0.375	29548	29548	(5+6)-I-3	2	--	Parz.
459.2	10.1	27.0	0.373	10.0	27.0	0.371	29548	29548	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
FLN	10.2	27.0	0.377	--	--	--	29548	29548	(3+4)-I-3	(5+6)-I-1	Parz.	--

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	12077	--	26274	19915	19915	0	29548	510.3	10.05	1.6
Des							29548			

Trave : 201 [208 , 209] Pilastrate [24 , 25]

Sez. R: By= 50.0 cm Bz=30.0 cm L=347.3 cm Ln=344.4 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	12028	9749	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	1.6
34.4	9135	8067	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	2.1
CAMP	7340	7482	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	2.5

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
310.0	9924	9471	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	1.9
FLN	12571	11400	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.5	27.0	0.389	10.4	27.0	0.385	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
34.4	10.4	27.0	0.384	10.3	27.0	0.382	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.381	10.3	27.0	0.382	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
310.0	10.4	27.0	0.386	10.4	27.0	0.385	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
FLN	10.4	27.0	0.384	10.5	27.0	0.388	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10834	--	16421	19915	16421	0	18798	344.4	10.05	1.5
Des							18798			

Trave : 201 [1, 206] Pilastrate [-, 23]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 145.0 \text{ cm}$ $L_n = 145.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	14	14	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	>100
14.5	22	14	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	>100
CAMP	328	--	--	--	14.07	14.07	18798	18798	1	(3+4)-I-1	57
130.5	415	--	--	--	14.07	14.07	18798	18798	1	(3+4)-I-1	45
FLN	512	--	--	--	14.07	14.07	18798	18798	1	(3+4)-I-1	37

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.0	27.0	0.371	10.0	27.0	0.371	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
14.5	10.0	27.0	0.371	10.0	27.0	0.371	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
CAMP	10.0	27.0	0.371	--	--	--	18798	18798	1	(3+4)-I-1	Parz.	--
130.5	10.0	27.0	0.371	--	--	--	18798	18798	1	(3+4)-I-1	Parz.	--
FLN	10.0	27.0	0.372	--	--	--	18798	18798	1	(3+4)-I-1	Parz.	--

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = 1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	707	--	16421	19915	16421	0	18798	145.0	10.05	23
Des							18798			

Trave : 201 [254, 255] Pilastrate [-, -]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 110.0 \text{ cm}$ $L_n = 110.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3396	3483	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	5.4
11.0	2630	2793	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	6.7
CAMP	2416	2539	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	7.4
99.0	3189	3224	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	5.8
FLN	3970	3898	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	4.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.1	27.0	0.375	10.1	27.0	0.376	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
11.0	10.1	27.0	0.374	10.1	27.0	0.375	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
CAMP	10.1	27.0	0.374	10.1	27.0	0.374	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
99.0	10.1	27.0	0.375	10.1	27.0	0.375	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
FLN	10.2	27.0	0.376	10.2	27.0	0.376	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	9482	--	16421	19915	16421	0	18798	110.0	10.05	1.7
Des							18798			

Trave : 201 | 209 , 2 | Pilastrate [25 , -]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 115.0 \text{ cm}$ $L_n = 115.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	322	--	--	--	14.07	14.07	18798	18798	2	(5+6)-I-3	58
11.5	261	--	--	--	14.07	14.07	18798	18798	2	(5+6)-I-3	72
CAMP	206	--	--	--	14.07	14.07	18798	18798	2	(5+6)-I-3	91
103.5	21	16	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	>100
FLN	16	16	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	>100

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.0	27.0	0.371	--	--	--	18798	18798	2	(5+6)-I-3	Parz.	--
11.5	10.0	27.0	0.371	--	--	--	18798	18798	2	(5+6)-I-3	Parz.	--
CAMP	10.0	27.0	0.371	--	--	--	18798	18798	2	(5+6)-I-3	Parz.	--
103.5	10.0	27.0	0.371	10.0	27.0	0.371	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.0	27.0	0.371	10.0	27.0	0.371	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	561	--	16421	19915	16421	0	18798	115.0	10.05	29
Des							18798			

Trave : 201 | 255 , 208 | Pilastrate [- , 24]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 100.0 \text{ cm}$ $L_n = 100.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3061	4354	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	4.3
10.0	3820	4877	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	3.9
CAMP	9556	8228	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	2.0
90.0	10429	8659	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	1.8
FLN	11307	9087	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	1.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.1	27.0	0.375	10.2	27.0	0.377	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
10.0	10.2	27.0	0.376	10.2	27.0	0.378	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
CAMP	10.4	27.0	0.385	10.3	27.0	0.383	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
90.0	10.4	27.0	0.386	10.4	27.0	0.383	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.5	27.0	0.388	10.4	27.0	0.384	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10950	--	16421	19915	16421	0	18798	100.0	10.05	1.5
Des							18798			

Trave : 201 [206 , 207] Pilastrate [23 , 30]

Sez. R: By= 50.0 cm Bz=30.0 cm L=347.3 cm Ln=344.4 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	11860	11037	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	1.6
34.4	9370	9183	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	2.0
CAMP	6939	7268	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	2.6
310.0	8738	7470	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	2.2
FLN	11524	9029	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.5	27.0	0.389	10.5	27.0	0.388	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
34.4	10.4	27.0	0.385	10.4	27.0	0.384	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.381	10.3	27.0	0.381	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
310.0	10.4	27.0	0.384	10.3	27.0	0.382	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.5	27.0	0.388	10.4	27.0	0.384	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10407	--	16421	19915	16421	0	18798	344.4	10.05	1.6
Des							18798			

Trave : 201 [207 , 254] Pilastrate [30 , -]

Sez. R: By= 50.0 cm Bz=30.0 cm L=100.0 cm Ln=100.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	11273	9505	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	1.7
10.0	10404	9058	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	1.8
CAMP	9546	8601	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	2.0
90.0	3876	5113	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	3.7
FLN	3119	4577	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	4.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.5	27.0	0.388	10.4	27.0	0.385	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
10.0	10.4	27.0	0.386	10.4	27.0	0.384	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.4	27.0	0.385	10.4	27.0	0.383	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
90.0	10.2	27.0	0.376	10.2	27.0	0.378	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
FLN	10.1	27.0	0.375	10.2	27.0	0.377	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10919	--	16421	19915	16421	0	18798	100.0	10.05	1.5
Des							18798			

Trave : 202 [220 , 216] Pilastrate [26 , 31]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 488.7 \text{ cm}$ $L_n = 488.7 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7699	3621	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	2.4
48.9	5525	3707	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.4
CAMP	3644	3587	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	5.2
439.9	3986	2082	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	4.7
FLN	6136	1913	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	3.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.382	10.1	27.0	0.376	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
48.9	10.2	27.0	0.379	10.1	27.0	0.376	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.1	27.0	0.376	10.1	27.0	0.376	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
439.9	10.2	27.0	0.376	10.1	27.0	0.374	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.2	27.0	0.379	10.1	27.0	0.373	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5379	--	16421	19915	16421	0	18798	488.7	10.05	3.1
Des							18798			

Trave : 202 [252 , 253] Pilastrate [- , -]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 110.0 \text{ cm}$ $L_n = 110.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1986	1328	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	9.5
11.0	1597	1044	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	12
CAMP	1399	633	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-I-1	13
99.0	1766	1308	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	11
FLN	2144	1607	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	8.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.1	27.0	0.374	10.1	27.0	0.373	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
11.0	10.1	27.0	0.373	10.1	27.0	0.372	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
CAMP	10.1	27.0	0.373	10.0	27.0	0.372	18798	18798	(5+6)-II-1	(3+4)-I-1	Parz.	Parz.
99.0	10.1	27.0	0.373	10.1	27.0	0.373	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	10.1	27.0	0.374	10.1	27.0	0.373	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4784	--	16421	19915	16421	0	18798	110.0	10.05	3.4
Des							18798			

Trave : 202 [212 , 206] Pilastrate [33 , 23]

Sez. R: By= 50.0 cm Bz=30.0 cm L=454.8 cm Ln=454.9 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6538	3082	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	2.9
45.5	4420	2882	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	4.3
CAMP	4285	4100	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	4.4
409.4	6228	4483	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	3.0
FLN	8439	4688	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	2.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.380	10.1	27.0	0.375	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
45.5	10.2	27.0	0.377	10.1	27.0	0.375	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.2	27.0	0.377	10.2	27.0	0.376	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
409.4	10.2	27.0	0.380	10.2	27.0	0.377	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.383	10.2	27.0	0.377	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5956	--	16421	19915	16421	0	18798	454.9	10.05	2.8
Des							18798			

Trave : 202 [216 , 252] Pilastrate [31 , -]

Sez. R: By= 50.0 cm Bz=30.0 cm L=100.0 cm Ln=100.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6140	3839	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.1
10.0	5597	3766	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.4
CAMP	5057	3689	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.7
90.0	1593	2841	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	6.6
FLN	1166	2674	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	7.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.379	10.2	27.0	0.376	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
10.0	10.2	27.0	0.379	10.2	27.0	0.376	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.2	27.0	0.378	10.1	27.0	0.376	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
90.0	10.1	27.0	0.373	10.1	27.0	0.375	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
FLN	10.1	27.0	0.372	10.1	27.0	0.374	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
Sin	6459	--	16421	19915	16421	0	18798	100.0	10.05	2.5
Des							18798			

Trave : 202 [253 , 212] Pilastrate [- , 33]

Sez. R: By= 50.0 cm Bz=30.0 cm L=100.0 cm Ln=100.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1031	2572	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	7.3
10.0	1447	2743	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	6.9
CAMP	4826	3612	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	3.9
90.0	5364	3683	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	3.5
FLN	5914	3741	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	3.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.1	27.0	0.372	10.1	27.0	0.374	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
10.0	10.1	27.0	0.373	10.1	27.0	0.375	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
CAMP	10.2	27.0	0.378	10.1	27.0	0.376	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
90.0	10.2	27.0	0.378	10.1	27.0	0.376	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.2	27.0	0.379	10.2	27.0	0.376	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio:cot(θ)=2.500

Comb =(3+4)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6561	--	16421	19915	16421	0	18798	100.0	10.05	2.5
Des							18798			

Trave : 203 [256 , 213] Pilastrate [- , 32]

Sez. R: By= 50.0 cm Bz=30.0 cm L=87.0 cm Ln=87.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1732	3241	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	5.8
8.7	2157	3410	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	5.5
CAMP	5505	4363	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	3.4
78.3	6025	4461	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	3.1
FLN	6556	4550	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	2.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.1	27.0	0.373	10.1	27.0	0.375	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
8.7	10.1	27.0	0.374	10.1	27.0	0.375	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
CAMP	10.2	27.0	0.379	10.2	27.0	0.377	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
78.3	10.2	27.0	0.379	10.2	27.0	0.377	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.380	10.2	27.0	0.377	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio:cot(θ)=2.500

Comb =(3+4)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7314	--	16421	19915	16421	0	18798	87.0	10.05	2.2
Des							18798			

Trave : 203 [223 , 217] Pilastrate [29 , 34]

Sez. R: By= 50.0 cm Bz=30.0 cm L=475.0 cm Ln=475.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7546	4708	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	2.5
47.5	5766	4339	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	3.3
CAMP	4093	3864	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	4.6
427.5	4260	2823	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	4.4
FLN	6366	2866	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	3.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.382	10.2	27.0	0.377	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
47.5	10.2	27.0	0.379	10.2	27.0	0.377	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
CAMP	10.2	27.0	0.376	10.2	27.0	0.376	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
427.5	10.2	27.0	0.377	10.1	27.0	0.375	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.380	10.1	27.0	0.375	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =(3+4)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5494	--	16421	19915	16421	0	18798	475.0	10.05	3.0
Des							18798			

Trave : 203 [217 , 257] Pilastrate [34 , -]

Sez. R: By= 50.0 cm Bz=30.0 cm L=87.0 cm Ln=87.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6740	4550	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	2.8
8.7	6212	4472	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.0
CAMP	5694	4384	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.3
78.3	2396	3503	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	5.4
FLN	1975	3340	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	5.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.380	10.2	27.0	0.377	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
8.7	10.2	27.0	0.380	10.2	27.0	0.377	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.2	27.0	0.379	10.2	27.0	0.377	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
78.3	10.1	27.0	0.374	10.1	27.0	0.376	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
FLN	10.1	27.0	0.373	10.1	27.0	0.375	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =(3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7267	--	16421	19915	16421	0	18798	87.0	10.05	2.3
Des							18798			

Trave : 203 [257 , 256] Pilastrate [- , -]

Sez. R: By= 50.0 cm Bz=30.0 cm L=136.0 cm Ln=136.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2733	2246	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	6.9
13.6	2182	1842	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	8.6
CAMP	1651	1284	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-I-3	11
122.4	2176	1895	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	8.6
FLN	2719	2305	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	6.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.1	27.0	0.375	10.1	27.0	0.374	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
13.6	10.1	27.0	0.374	10.1	27.0	0.373	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
CAMP	10.1	27.0	0.373	10.1	27.0	0.373	18798	18798	(5+6)-II-1	(3+4)-I-3	Parz.	Parz.
122.4	10.1	27.0	0.374	10.1	27.0	0.373	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	10.1	27.0	0.375	10.1	27.0	0.374	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5479	--	16421	19915	16421	0	18798	136.0	10.05	3.0
Des							18798			

Trave : 204 [213 , 209] Pilastrate [32 , 25]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 460.1 \text{ cm}$ $L_n = 460.2 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5937	2721	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.2
46.0	4016	2598	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	4.7
CAMP	4030	3802	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	4.7
414.2	5802	4148	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	3.2
FLN	7805	4333	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	2.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.379	10.1	27.0	0.375	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
46.0	10.2	27.0	0.376	10.1	27.0	0.374	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
CAMP	10.2	27.0	0.376	10.2	27.0	0.376	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
414.2	10.2	27.0	0.379	10.2	27.0	0.377	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.382	10.2	27.0	0.377	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5329	--	16421	19915	16421	0	18798	460.2	10.05	3.1
Des							18798			

Trave : 205 [3 , 220] Pilastrate [- , 26]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 145.0 \text{ cm}$ $L_n = 145.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7	7	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	>100

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
14.5	13	5	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	>100
CAMP	328	--	--	--	14.07	14.07	18798	18798	1	(5+6)-I-1	57
130.5	415	--	--	--	14.07	14.07	18798	18798	1	(5+6)-I-1	45
FLN	512	--	--	--	14.07	14.07	18798	18798	1	(5+6)-I-3	37

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.0	27.0	0.371	10.0	27.0	0.371	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
14.5	10.0	27.0	0.371	10.0	27.0	0.371	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.0	27.0	0.371	--	--	--	18798	18798	1	(5+6)-I-1	Parz.	--
130.5	10.0	27.0	0.371	--	--	--	18798	18798	1	(5+6)-I-1	Parz.	--
FLN	10.0	27.0	0.372	--	--	--	18798	18798	1	(5+6)-I-3	Parz.	--

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = 1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	707	--	16421	19915	16421	0	18798	145.0	10.05	23
Des							18798			

Trave : 205 [220 , 221] Pilastrate [26 , 27]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 345.0 \text{ cm}$ $L_n = 345.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	8014	7331	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	2.3
34.5	6284	6155	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	3.0
CAMP	4605	4926	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	3.8
310.5	6032	4785	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	3.1
FLN	8062	5662	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	2.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.382	10.3	27.0	0.381	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
34.5	10.3	27.0	0.380	10.2	27.0	0.379	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
CAMP	10.2	27.0	0.377	10.2	27.0	0.378	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
310.5	10.2	27.0	0.379	10.2	27.0	0.377	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.3	27.0	0.382	10.2	27.0	0.379	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7487	--	16421	19915	16421	0	18798	345.0	10.05	2.2
Des							18798			

Trave : 205 [221 , 251] Pilastrate [27 , -]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 92.0 \text{ cm}$ $L_n = 92.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7749	6413	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	2.4
9.2	7125	6211	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	2.6
CAMP	6511	5998	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	2.9
82.8	2601	4243	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	4.4

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
FLN	2092	3944	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	4.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.382	10.3	27.0	0.380	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
9.2	10.3	27.0	0.381	10.2	27.0	0.380	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.380	10.2	27.0	0.379	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
82.8	10.1	27.0	0.374	10.2	27.0	0.377	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
FLN	10.1	27.0	0.374	10.2	27.0	0.376	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8321	--	16421	19915	16421	0	18798	92.0	10.05	2.0
Des							18798			

Trave : 205 [251 , 250] Pilastrate [- , -]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 126.0 \text{ cm}$ $L_n = 126.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2584	2472	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	7.3
12.6	1970	1933	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	9.5
CAMP	2312	2042	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	8.1
113.4	2957	2547	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	6.4
FLN	3614	3037	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	5.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.1	27.0	0.374	10.1	27.0	0.374	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
12.6	10.1	27.0	0.373	10.1	27.0	0.373	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
CAMP	10.1	27.0	0.374	10.1	27.0	0.374	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
113.4	10.1	27.0	0.375	10.1	27.0	0.374	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
FLN	10.1	27.0	0.376	10.1	27.0	0.375	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6960	--	16421	19915	16421	0	18798	126.0	10.05	2.4
Des							18798			

Trave : 205 [250 , 222] Pilastrate [- , 28]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 92.0 \text{ cm}$ $L_n = 92.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2537	3832	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	4.9
9.2	3068	4107	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	4.6
CAMP	7209	5754	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	2.6
82.8	7852	5945	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	2.4
FLN	8508	6124	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	2.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.1	27.0	0.374	10.2	27.0	0.376	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
9.2	10.1	27.0	0.375	10.2	27.0	0.376	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
CAMP	10.3	27.0	0.381	10.2	27.0	0.379	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
82.8	10.3	27.0	0.382	10.2	27.0	0.379	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.3	27.0	0.383	10.2	27.0	0.379	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8672	--	16421	19915	16421	0	18798	92.0	10.05	1.9
Des							18798			

Trave : 205 [222 , 223] Pilastrate [28 , 29]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 480.0 \text{ cm}$ $L_n = 480.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7217	3630	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	2.6
48.0	5029	3578	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	3.7
CAMP	3689	3393	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	5.1
432.0	5450	3874	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	3.4
FLN	7326	4239	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	2.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.381	10.1	27.0	0.376	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
48.0	10.2	27.0	0.378	10.1	27.0	0.376	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.1	27.0	0.376	10.1	27.0	0.375	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
432.0	10.2	27.0	0.378	10.2	27.0	0.376	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
FLN	10.3	27.0	0.381	10.2	27.0	0.377	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5654	--	16421	19915	16421	0	18798	480.0	10.05	2.9
Des							18798			

Trave : 206 [253 , 254] Pilastrate [- , -]

Sez. R: $B_y = 20.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 806.2 \text{ cm}$ $L_n = 792.1 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1631	57	--	--	6.03	6.03	8048	8048	(5+6)-I-3	(3+4)-I-1	4.9
79.2	1082	399	--	--	6.03	6.03	8048	8048	(5+6)-I-3	(3+4)-I-1	7.4
CAMP	630	845	--	--	6.03	6.03	8048	8048	(5+6)-I-3	(3+4)-I-1	9.5
712.9	1116	324	--	--	6.03	6.03	8048	8048	(3+4)-II-1	(5+6)-II-2	7.2
FLN	1725	--	--	--	6.03	6.03	8048	8048	(3+4)-II-1	(5+6)-II-2	4.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.382	10.2	27.0	0.377	8048	8048	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
79.2	10.3	27.0	0.381	10.2	27.0	0.378	8048	8048	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	10.2	27.0	0.379	10.3	27.0	0.380	8048	8048	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
712.9	10.3	27.0	0.381	10.2	27.0	0.378	8048	8048	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.383	--	--	--	8048	8048	(3+4)-II-1	(5+6)-II-2	Parz.	--

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	943	--	6568	9957	6568	0	8048	792.1	5.03	7.0
Des							8048			

Trave : 207 [251 , 252] Pilastrate [- , -]

Sez. R: $B_y = 20.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 797.1 \text{ cm}$ $L_n = 790.2 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1677	--	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	4.8
79.0	1064	276	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	7.6
CAMP	657	820	--	--	6.03	6.03	8048	8048	(5+6)-I-3	(3+4)-II-1	9.8
711.2	1169	435	--	--	6.03	6.03	8048	8048	(5+6)-I-3	(3+4)-I-1	6.9
FLN	1780	116	--	--	6.03	6.03	8048	8048	(5+6)-I-3	(3+4)-I-1	4.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.383	--	--	--	8048	8048	(3+4)-II-2	(5+6)-II-1	Parz.	--
79.0	10.3	27.0	0.381	10.2	27.0	0.378	8048	8048	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.2	27.0	0.379	10.3	27.0	0.380	8048	8048	(5+6)-I-3	(3+4)-II-1	Parz.	Parz.
711.2	10.3	27.0	0.381	10.2	27.0	0.379	8048	8048	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
FLN	10.3	27.0	0.383	10.2	27.0	0.378	8048	8048	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1036	--	6568	9957	6568	0	8048	790.2	5.03	6.3
Des							8048			

Trave : 208 [250 , 257] Pilastrate [- , -]

Sez. R: $B_y = 20.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 801.8 \text{ cm}$ $L_n = 794.7 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1679	80	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	4.8
79.5	1114	381	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	7.2
CAMP	644	793	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-I-3	10
715.2	1078	455	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	7.5
FLN	1617	155	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	5.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.383	10.2	27.0	0.377	8048	8048	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
79.5	10.3	27.0	0.381	10.2	27.0	0.378	8048	8048	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.2	27.0	0.379	10.3	27.0	0.380	8048	8048	(3+4)-II-2	(5+6)-I-3	Parz.	Parz.
715.2	10.3	27.0	0.381	10.2	27.0	0.379	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.3	27.0	0.382	10.2	27.0	0.378	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	828	--	6568	9957	6568	0	8048	794.7	5.03	7.9
Des							8048			

Trave : 209 [256 , 255] Pilastrate [- , -]

Sez. R: By= 20.0 cm Bz=30.0 cm L=810.8 cm Ln=796.7 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1726	137	--	--	6.03	6.03	8048	8048	(5+6)-I-1	(3+4)-I-3	4.7
79.7	1132	453	--	--	6.03	6.03	8048	8048	(5+6)-I-1	(3+4)-I-3	7.1
CAMP	644	780	--	--	6.03	6.03	8048	8048	(5+6)-I-1	(5+6)-I-3	10
717.0	1037	253	--	--	6.03	6.03	8048	8048	(3+4)-II-1	(5+6)-II-2	7.8
FLN	1576	--	--	--	6.03	6.03	8048	8048	(3+4)-II-1	(5+6)-II-2	5.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.383	10.2	27.0	0.378	8048	8048	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
79.7	10.3	27.0	0.381	10.2	27.0	0.379	8048	8048	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
CAMP	10.2	27.0	0.379	10.3	27.0	0.380	8048	8048	(5+6)-I-1	(5+6)-I-3	Parz.	Parz.
717.0	10.3	27.0	0.381	10.2	27.0	0.378	8048	8048	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.382	--	--	--	8048	8048	(3+4)-II-1	(5+6)-II-2	Parz.	--

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (5+6)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	872	--	6568	9957	6568	0	8048	796.7	5.03	7.5
Des							8048			

Trave : 301 [301 , 302] Pilastrate [1 , 2]

Sez. R: By= 50.0 cm Bz=30.0 cm L=835.0 cm Ln=835.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7362	3412	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	2.6
83.5	5128	3445	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	3.7
CAMP	3680	3226	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	5.1
751.5	5740	3371	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	3.3
FLN	8062	3254	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	2.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.381	10.1	27.0	0.375	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
83.5	10.2	27.0	0.378	10.1	27.0	0.376	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.1	27.0	0.376	10.1	27.0	0.375	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
751.5	10.2	27.0	0.379	10.1	27.0	0.375	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.3	27.0	0.382	10.1	27.0	0.375	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3377	--	16421	19915	16421	0	18798	835.0	10.05	4.9
Des							18798			

Trave : 302 [303 , 304] Pilastrate [3 , 4]

Sez. R: By= 50.0 cm Bz=30.0 cm L=835.0 cm Ln=835.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²], fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	8034	3437	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	2.3
83.5	5719	3513	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	3.3
CAMP	3666	3328	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	5.1
751.5	5309	3404	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	3.5
FLN	7583	3363	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	2.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.382	10.1	27.0	0.376	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
83.5	10.2	27.0	0.379	10.1	27.0	0.376	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.1	27.0	0.376	10.1	27.0	0.375	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
751.5	10.2	27.0	0.378	10.1	27.0	0.375	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.3	27.0	0.382	10.1	27.0	0.375	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: cot(θ) = 2.500

Comb =(3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3375	--	16421	19915	16421	0	18798	835.0	10.05	4.9
Des							18798			

Trave : 303 [325 , 324] Pilastrate [14 , 15]

Sez. R: By= 60.0 cm Bz=30.0 cm L=450.0 cm Ln=450.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²], fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7469	3027	--	--	18.10	18.10	24144	24144	(3+4)-II-2	(5+6)-II-1	3.2
45.0	5269	3254	--	--	18.10	18.10	24144	24144	(3+4)-II-2	(5+6)-II-1	4.6
CAMP	3243	3307	--	--	18.10	18.10	24144	24144	(3+4)-II-2	(5+6)-II-1	7.3
405.0	5177	2084	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	4.7
FLN	8068	1166	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	3.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.385	10.3	27.0	0.380	24144	24144	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
45.0	10.3	27.0	0.383	10.3	27.0	0.381	24144	24144	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.3	27.0	0.381	10.3	27.0	0.381	24144	24144	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
405.0	10.3	27.0	0.383	10.2	27.0	0.379	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	10.4	27.0	0.386	10.2	27.0	0.378	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: cot(θ) = 2.500

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8443	--	19705	19915	19705	0	24144	450.0	10.05	2.3
Des							24144			

Trave : 303 [324 , 0] Pilastrate [15 , -]

Sez. R: By= 60.0 cm Bz=30.0 cm L=315.0 cm Ln=315.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	8490	1155	--	--	18.10	18.10	24144	24144	(5+6)-II-2	(3+4)-II-1	2.8
31.5	6370	1932	--	--	18.10	18.10	24144	24144	(5+6)-II-2	(3+4)-II-1	3.8
CAMP	4467	3431	--	--	18.10	18.10	24144	24144	(5+6)-II-2	2	5.4
283.5	--	2869	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	8.4
FLN	734	3072	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	7.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.387	10.2	27.0	0.378	24144	24144	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
31.5	10.4	27.0	0.384	10.2	27.0	0.379	24144	24144	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
CAMP	10.3	27.0	0.382	10.3	27.0	0.381	24144	24144	(5+6)-II-2	2	Parz.	Parz.
283.5	--	--	--	10.3	27.0	0.380	24144	24144	(5+6)-II-1	(3+4)-II-2	--	Parz.
FLN	10.2	27.0	0.378	10.3	27.0	0.380	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8785	--	19705	19915	19705	0	24144	315.0	10.05	2.2
Des							24144			

Trave : 303 [0 , 319] Pilastrate [- , 16]

Sez. R: By= 60.0 cm Bz=30.0 cm L=155.0 cm Ln=155.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	88	3004	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	8.0
15.5	709	2949	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	8.2
CAMP	5370	2884	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	4.5
139.5	6079	2130	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	4.0
FLN	6799	1979	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	3.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.377	10.3	27.0	0.380	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
15.5	10.2	27.0	0.378	10.3	27.0	0.380	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
CAMP	10.3	27.0	0.383	10.3	27.0	0.380	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
139.5	10.4	27.0	0.384	10.2	27.0	0.379	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	10.4	27.0	0.385	10.2	27.0	0.379	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =(3+4)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5310	--	19797	19915	19797	0	24144	155.0	10.05	3.7
Des							24144			

Trave : 303 [319 , 315] Pilastrate [16 , 17]

Sez. R: By= 50.0 cm Bz=30.0 cm L=450.0 cm Ln=450.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5
::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5814	3582	--	--	18.10	18.10	24093	24093	(5+6)-II-2	(3+4)-II-1	4.1
45.0	4392	2978	--	--	18.10	18.10	24093	24093	(5+6)-II-2	(3+4)-II-1	5.5
CAMP	3382	3432	--	--	18.10	18.10	24093	24093	(3+4)-II-1	(5+6)-II-2	7.0
405.0	4594	4246	--	--	18.10	18.10	24093	24093	(3+4)-II-1	(5+6)-II-2	5.2
FLN	5882	4984	--	--	18.10	18.10	24093	24093	(3+4)-II-1	(5+6)-II-2	4.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.8	27.0	0.400	10.7	27.0	0.398	24093	24093	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
45.0	10.8	27.0	0.399	10.7	27.0	0.397	24093	24093	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
CAMP	10.7	27.0	0.397	10.7	27.0	0.397	24093	24093	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
405.0	10.8	27.0	0.399	10.8	27.0	0.398	24093	24093	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.8	27.0	0.400	10.8	27.0	0.399	24093	24093	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

*Verifica a taglio:*cot(θ) =2.500

Comb =(5+6)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3993	--	16421	19915	16421	0	24093	450.0	10.05	4.1
Des							24093			

Trave : 304 [311 , 305] Pilastrate [18 , 9]

Sez. R: By= 50.0 cm Bz=30.0 cm L=440.0 cm Ln=440.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5
::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5889	5191	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.2
44.0	4618	4395	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	4.1
CAMP	3421	3525	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	5.3
396.0	4593	2930	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	4.1
FLN	6043	3546	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	3.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.379	10.2	27.0	0.378	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
44.0	10.2	27.0	0.377	10.2	27.0	0.377	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.1	27.0	0.375	10.1	27.0	0.376	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
396.0	10.2	27.0	0.377	10.1	27.0	0.375	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	10.2	27.0	0.379	10.1	27.0	0.376	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.

*Verifica a taglio:*cot(θ) =2.500

Comb =(5+6)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4159	--	16421	19915	16421	0	18798	440.0	10.05	3.9
Des							18798			

Trave : 304 [305 , 0] Pilastrate [9 , -]

Sez. R: By= 60.0 cm Bz=30.0 cm L=155.0 cm Ln=155.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5
::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
ILN	7194	761	--	--	14.07	14.07	18858	18858	(3+4)-II-2	(5+6)-II-1	2.6
15.5	6416	1013	--	--	14.07	14.07	18858	18858	(3+4)-II-2	(5+6)-II-1	2.9
CAMP	5649	2474	--	--	14.07	14.07	18858	18858	(3+4)-II-2	(5+6)-II-1	3.3
139.5	587	2642	--	--	14.07	14.07	18858	18858	(3+4)-II-2	(5+6)-II-1	7.1
FLN	--	2799	--	--	14.07	14.07	18858	18858	(3+4)-II-2	(5+6)-II-1	6.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.8	27.0	0.363	9.6	27.0	0.355	18858	18858	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
15.5	9.8	27.0	0.362	9.6	27.0	0.355	18858	18858	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	9.8	27.0	0.361	9.6	27.0	0.357	18858	18858	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
139.5	9.6	27.0	0.355	9.6	27.0	0.357	18858	18858	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
FLN	--	--	--	9.6	27.0	0.357	18858	18858	(3+4)-II-2	(5+6)-II-1	--	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5628	--	19705	19915	19705	0	18858	155.0	10.05	3.5
Des							18858			

Trave : 304 [0 , 301] Pilastrate [- , 1]

Sez. R: $B_y = 60.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 315.1 \text{ cm}$ $L_n = 314.6 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	776	3152	--	--	14.07	14.07	18858	18858	(3+4)-II-2	(5+6)-II-1	6.0
31.5	--	3174	--	--	14.07	14.07	18858	18858	(3+4)-II-2	(5+6)-II-1	5.9
CAMP	--	4253	--	--	14.07	14.07	18858	18858	(3+4)-I-1	2	4.4
283.2	4324	2585	--	--	14.07	14.07	18858	18858	(3+4)-II-1	(5+6)-II-2	4.4
FLN	6227	1880	--	--	14.07	14.07	18858	18858	(3+4)-II-1	(5+6)-II-2	3.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	9.6	27.0	0.355	9.7	27.0	0.358	18858	18858	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
31.5	--	--	--	9.7	27.0	0.358	18858	18858	(3+4)-II-2	(5+6)-II-1	--	Parz.
CAMP	--	--	--	9.7	27.0	0.359	18858	18858	(3+4)-I-1	2	--	Parz.
283.2	9.7	27.0	0.359	9.6	27.0	0.357	18858	18858	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	9.8	27.0	0.362	9.6	27.0	0.356	18858	18858	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7979	--	19705	19915	19705	0	18858	314.6	10.05	2.5
Des							18858			

Trave : 305 [330 , 318] Pilastrate [13 , 12]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 600.0 \text{ cm}$ $L_n = 600.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6158	3702	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.1
60.0	4524	3306	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	4.2
CAMP	3258	3145	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	5.8

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
540.0	4731	3695	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	4.0
FLN	6339	4111	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	3.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.379	10.1	27.0	0.376	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
60.0	10.2	27.0	0.377	10.1	27.0	0.375	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.1	27.0	0.375	10.1	27.0	0.375	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
540.0	10.2	27.0	0.377	10.1	27.0	0.376	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.380	10.2	27.0	0.376	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3398	--	16421	19915	16421	0	18798	600.0	10.05	4.8
Des							18798			

Trave : 306 [0 , 304] Pilastrate [- , 4]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 315.1 \text{ cm}$ $L_n = 314.7 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	992	3242	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	5.8
31.5	--	3209	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	5.9
CAMP	--	4003	--	--	14.07	14.07	18798	18798	(3+4)-I-3	2	4.7
283.3	4556	2424	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	4.1
FLN	6461	1757	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	2.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.0	27.0	0.372	10.1	27.0	0.375	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
31.5	--	--	--	10.1	27.0	0.375	18798	18798	(3+4)-II-2	(5+6)-II-1	--	Parz.
CAMP	--	--	--	10.2	27.0	0.376	18798	18798	(3+4)-I-3	2	--	Parz.
283.3	10.2	27.0	0.377	10.1	27.0	0.374	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.380	10.1	27.0	0.373	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7934	--	16421	19915	16421	0	18798	314.7	10.05	2.1
Des							18798			

Trave : 306 [314 , 310] Pilastrate [11 , 10]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 440.0 \text{ cm}$ $L_n = 440.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6331	5822	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.0
44.0	4970	4901	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.8
CAMP	3681	3907	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	4.8
396.0	5083	3305	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	3.7
FLN	6657	4013	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	2.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.380	10.2	27.0	0.379	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
44.0	10.2	27.0	0.378	10.2	27.0	0.378	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.1	27.0	0.376	10.2	27.0	0.376	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
396.0	10.2	27.0	0.378	10.1	27.0	0.375	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.380	10.2	27.0	0.376	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4524	--	16421	19915	16421	0	18798	440.0	10.05	3.6
Des							18798			

Trave : 306 [310 , 0] Pilastrate [10 , -]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 155.1 \text{ cm}$ $L_n = 155.2 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6669	749	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	2.8
15.5	5950	982	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	3.2
CAMP	5240	2384	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	3.6
139.7	564	2559	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	7.3
FLN	--	2731	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	6.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.380	10.0	27.0	0.372	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
15.5	10.2	27.0	0.379	10.0	27.0	0.372	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
CAMP	10.2	27.0	0.378	10.1	27.0	0.374	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
139.7	10.0	27.0	0.372	10.1	27.0	0.374	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
FLN	--	--	--	10.1	27.0	0.375	18798	18798	(5+6)-II-2	(3+4)-II-1	--	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5251	--	16421	19915	16421	0	18798	155.2	10.05	3.1
Des							18798			

Trave : 307 [325 , 326] Pilastrate [14 , 7]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 444.9 \text{ cm}$ $L_n = 453.7 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3420	2798	--	--	18.10	18.10	24093	24093	(3+4)-I-3	(5+6)-I-1	7.0
45.4	2440	2542	--	--	18.10	18.10	24093	24093	(3+4)-I-3	(5+6)-I-1	9.5
CAMP	1441	2201	--	--	18.10	18.10	24093	24093	(5+6)-II-1	(5+6)-I-1	11
408.4	3094	1804	--	--	18.10	18.10	24093	24093	(5+6)-I-1	(3+4)-I-3	7.8
FLN	4338	1794	--	--	18.10	18.10	24093	24093	(5+6)-I-1	(3+4)-I-3	5.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.7	27.0	0.397	10.7	27.0	0.397	24093	24093	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
45.4	10.7	27.0	0.396	10.7	27.0	0.396	24093	24093	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.7	27.0	0.395	10.7	27.0	0.396	24093	24093	(5+6)-II-1	(5+6)-I-1	Parz.	Parz.
408.4	10.7	27.0	0.397	10.7	27.0	0.396	24093	24093	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
FLN	10.8	27.0	0.399	10.7	27.0	0.396	24093	24093	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3346	--	16421	19915	16421	0	24093	453.7	10.05	4.9
Des							24093			

Trave : 307 [326 , 327] Pilastrate [7 , 6]

Sez. R: By= 50.0 cm Bz=30.0 cm L=450.0 cm Ln=450.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	4814	2447	--	--	18.10	18.10	24093	24093	(5+6)-I-3	(3+4)-I-1	5.0
45.0	3392	2369	--	--	18.10	18.10	24093	24093	(5+6)-I-3	(3+4)-I-1	7.1
CAMP	2594	2151	--	--	18.10	18.10	24093	24093	(3+4)-I-1	(5+6)-I-3	9.3
405.0	4006	2240	--	--	18.10	18.10	24093	24093	(3+4)-I-1	(5+6)-I-3	6.0
FLN	5612	2135	--	--	18.10	18.10	24093	24093	(3+4)-I-1	(5+6)-I-3	4.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.8	27.0	0.399	10.7	27.0	0.396	24093	24093	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
45.0	10.7	27.0	0.397	10.7	27.0	0.396	24093	24093	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
CAMP	10.7	27.0	0.397	10.7	27.0	0.396	24093	24093	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
405.0	10.7	27.0	0.398	10.7	27.0	0.396	24093	24093	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.8	27.0	0.400	10.7	27.0	0.396	24093	24093	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4339	--	16421	19915	16421	0	24093	450.0	10.05	3.8
Des							24093			

Trave : 308 [328 , 329] Pilastrate [5 , 8]

Sez. R: By= 50.0 cm Bz=30.0 cm L=517.0 cm Ln=517.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5787	1670	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	3.2
51.7	3737	2277	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	5.0
CAMP	2022	2549	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	7.4
465.3	4139	1410	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	4.5
FLN	6206	786	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	3.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.379	10.1	27.0	0.373	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
51.7	10.2	27.0	0.376	10.1	27.0	0.374	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.1	27.0	0.374	10.1	27.0	0.374	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
465.3	10.2	27.0	0.377	10.1	27.0	0.373	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
FLN	10.2	27.0	0.380	10.0	27.0	0.372	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4996	--	16421	19915	16421	0	18798	517.0	10.05	3.3
Des							18798			

Trave : 308 [329 , 330] Pilastrate [8 , 13]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 395.2 \text{ cm}$ $L_n = 386.1 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6163	1056	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	3.1
38.6	4152	1680	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	4.5
CAMP	--	2540	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-I-3	7.4
347.5	2778	2489	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	6.8
FLN	4456	2197	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	4.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.380	10.1	27.0	0.372	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
38.6	10.2	27.0	0.377	10.1	27.0	0.373	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	--	--	--	10.1	27.0	0.374	18798	18798	(5+6)-II-1	(3+4)-I-3	--	Parz.
347.5	10.1	27.0	0.375	10.1	27.0	0.374	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
FLN	10.2	27.0	0.377	10.1	27.0	0.374	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = 2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6760	--	16421	19915	16421	0	18798	386.1	10.05	2.4
Des							18798			

Trave : 309 [0 , 307] Pilastrate [-, 30]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 125.1 \text{ cm}$ $L_n = 125.6 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2219	3669	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	5.1
12.6	2878	3549	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	5.3
CAMP	7664	3424	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	2.5
113.0	8371	2383	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	2.2
FLN	9085	2211	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	2.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.1	27.0	0.374	10.1	27.0	0.376	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
12.6	10.1	27.0	0.375	10.1	27.0	0.376	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
CAMP	10.3	27.0	0.382	10.1	27.0	0.375	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
113.0	10.3	27.0	0.383	10.1	27.0	0.374	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
FLN	10.4	27.0	0.384	10.1	27.0	0.374	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6428	--	16421	19915	16421	0	18798	125.6	10.05	2.6
Des							18798			

Trave : 309 [302 , 0] Pilastrate [2 , -]

Sez. R: By= 50.0 cm Bz=30.0 cm L=315.1 cm Ln=314.8 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6015	2425	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	3.1
31.5	4083	2837	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	4.6
CAMP	--	3719	--	--	14.07	14.07	18798	18798	(3+4)-I-3	2	5.1
283.3	1380	3871	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	4.9
FLN	2826	3942	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	4.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.379	10.1	27.0	0.374	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
31.5	10.2	27.0	0.376	10.1	27.0	0.375	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
CAMP	--	--	--	10.1	27.0	0.376	18798	18798	(3+4)-I-3	2	--	Parz.
283.3	10.1	27.0	0.373	10.2	27.0	0.376	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
FLN	10.1	27.0	0.375	10.2	27.0	0.376	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7276	--	16421	19915	16421	0	18798	314.8	10.05	2.3
Des							18798			

Trave : 310 [0 , 308] Pilastrate [- , 24]

Sez. R: By= 50.0 cm Bz=30.0 cm L=125.0 cm Ln=118.8 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2619	3701	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	5.1
11.9	3266	3616	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	5.2
CAMP	7951	3527	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	2.4
106.9	8642	2759	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	2.2
FLN	9339	2629	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	2.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.1	27.0	0.374	10.1	27.0	0.376	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
11.9	10.1	27.0	0.375	10.1	27.0	0.376	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
CAMP	10.3	27.0	0.382	10.1	27.0	0.376	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
106.9	10.4	27.0	0.383	10.1	27.0	0.375	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
FLN	10.4	27.0	0.385	10.1	27.0	0.374	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
Sin	6686	--	16421	19915	16421	0	18798	118.8	10.05	2.5
Des							18798			

Trave : 310 [303 , 0] Pilastrate [3 , -]

Sez. R: By= 50.0 cm Bz=30.0 cm L=315.1 cm Ln=299.7 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5568	2954	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	3.4
30.0	3753	3209	--	--	14.07	14.07	18798	18798	(3+4)-II-1	(5+6)-II-2	5.0
CAMP	--	3656	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-II-1	5.1
269.7	1557	3965	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	4.7
FLN	2987	4090	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-II-1	4.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.379	10.1	27.0	0.375	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
30.0	10.2	27.0	0.376	10.1	27.0	0.375	18798	18798	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
CAMP	--	--	--	10.1	27.0	0.376	18798	18798	(3+4)-I-1	(5+6)-II-1	--	Parz.
269.7	10.1	27.0	0.373	10.2	27.0	0.376	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
FLN	10.1	27.0	0.375	10.2	27.0	0.376	18798	18798	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.

Verifica a taglio:cot(θ)=2.500

Comb =(3+4)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7242	--	16421	19915	16421	0	18798	299.7	10.05	2.3
Des							18798			

Trave : 311 [305 , 0] Pilastrate [9 , -]

Sez. R: By= 60.0 cm Bz=30.0 cm L=253.0 cm Ln=252.4 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	8059	3817	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	3.0
25.2	6519	4093	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	3.7
CAMP	5089	4315	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	4.7
227.1	--	3276	--	--	18.10	18.10	24144	24144	(3+4)-II-2		2 7.4
FLN	--	3062	--	--	18.10	18.10	24144	24144	(3+4)-I-1		2 7.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.386	10.3	27.0	0.381	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
25.2	10.4	27.0	0.384	10.3	27.0	0.382	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.383	10.3	27.0	0.382	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
227.1	--	--	--	10.3	27.0	0.381	24144	24144	(3+4)-II-2	2	--	Parz.
FLN	--	--	--	10.3	27.0	0.380	24144	24144	(3+4)-I-1	2	--	Parz.

Verifica a taglio:cot(θ)=2.500

Comb =(3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7155	--	19705	19915	19705	0	24144	252.4	10.05	2.8
Des							24144			

Trave : 311 | 0, 306 | Pilastrate [- , 23]

Sez. R: By= 60.0 cm Bz=30.0 cm L=257.1 cm Ln=256.3 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	3550	--	--	14.07	14.07	18858	18858	(3+4)-II-2	2	5.3
25.6	--	2924	--	--	14.07	14.07	18858	18858	(3+4)-I-1	2	6.4
CAMP	7428	4293	--	--	14.07	14.07	18858	18858	(5+6)-I-1	(3+4)-I-3	2.5
230.6	8795	4426	--	--	14.07	14.07	18858	18858	(5+6)-I-1	(3+4)-I-3	2.1
FLN	10192	4529	--	--	14.07	14.07	18858	18858	(5+6)-I-1	(3+4)-I-3	1.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	9.7	27.0	0.358	18858	18858	(3+4)-II-2	2	--	Parz.
25.6	--	--	--	9.7	27.0	0.358	18858	18858	(3+4)-I-1	2	--	Parz.
CAMP	9.8	27.0	0.364	9.7	27.0	0.359	18858	18858	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
230.6	9.9	27.0	0.366	9.7	27.0	0.360	18858	18858	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
FLN	9.9	27.0	0.368	9.7	27.0	0.360	18858	18858	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =(5+6)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6486	--	19705	19915	19705	0	18858	256.3	10.05	3.0
Des							18858			

Trave : 312 | 0, 309 | Pilastrate [- , 25]

Sez. R: By= 60.0 cm Bz=30.0 cm L=257.1 cm Ln=256.3 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	3494	--	--	18.10	18.10	24144	24144	(3+4)-II-1	2	6.9
25.6	--	2876	--	--	18.10	18.10	24144	24144	(3+4)-II-2	2	8.4
CAMP	7474	4325	--	--	18.10	18.10	24144	24144	(5+6)-I-3	(3+4)-I-1	3.2
230.6	8869	4493	--	--	18.10	18.10	24144	24144	(5+6)-I-3	(3+4)-I-1	2.7
FLN	10293	4632	--	--	18.10	18.10	24144	24144	(5+6)-I-3	(3+4)-I-1	2.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	10.3	27.0	0.381	24144	24144	(3+4)-II-1	2	--	Parz.
25.6	--	--	--	10.3	27.0	0.380	24144	24144	(3+4)-II-2	2	--	Parz.
CAMP	10.4	27.0	0.385	10.3	27.0	0.382	24144	24144	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
230.6	10.5	27.0	0.387	10.3	27.0	0.382	24144	24144	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
FLN	10.5	27.0	0.389	10.3	27.0	0.382	24144	24144	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =(5+6)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6638	--	19705	19915	19705	0	24144	256.3	10.05	3.0
Des							24144			

Trave : 312 | 310, 0 | Pilastrate [10, -]

Sez. R: By= 60.0 cm Bz=30.0 cm L=253.0 cm Ln=252.4 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7922	3587	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	3.0
25.2	6396	3885	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	3.8
CAMP	4980	4153	--	--	18.10	18.10	24144	24144	(3+4)-I-1	(5+6)-I-3	4.8
227.1	--	3272	--	--	18.10	18.10	24144	24144	(3+4)-II-2	2	7.4
FLN	--	3066	--	--	18.10	18.10	24144	24144	(3+4)-II-2	2	7.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.386	10.3	27.0	0.381	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
25.2	10.4	27.0	0.384	10.3	27.0	0.381	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
CAMP	10.3	27.0	0.383	10.3	27.0	0.382	24144	24144	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
227.1	--	--	--	10.3	27.0	0.381	24144	24144	(3+4)-II-2	2	--	Parz.
FLN	--	--	--	10.3	27.0	0.380	24144	24144	(3+4)-II-2	2	--	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7073	--	19705	19915	19705	0	24144	252.4	10.05	2.8
Des							24144			

Trave : 313 [0 , 313] Pilastrate [- , 32]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 122.6 \text{ cm}$ $L_n = 122.6 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1458	2623	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	7.2
12.3	1924	2720	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	6.9
CAMP	5372	3266	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	3.5
110.3	5889	3323	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	3.2
FLN	6411	3374	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	2.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.1	27.0	0.373	10.1	27.0	0.374	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
12.3	10.1	27.0	0.373	10.1	27.0	0.375	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.2	27.0	0.378	10.1	27.0	0.375	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
110.3	10.2	27.0	0.379	10.1	27.0	0.375	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
FLN	10.3	27.0	0.380	10.1	27.0	0.375	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5075	--	16421	19915	16421	0	18798	122.6	10.05	3.2
Des							18798			

Trave : 313 [314 , 0] Pilastrate [11 , -]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 253.0 \text{ cm}$ $L_n = 252.4 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5899	4361	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	3.2

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
25.2	4721	4133	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	4.0
CAMP	3624	3825	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	4.9
227.2	602	1858	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	10
FLN	1545	2310	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	8.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.379	10.2	27.0	0.377	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
25.2	10.2	27.0	0.377	10.2	27.0	0.377	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
CAMP	10.1	27.0	0.376	10.2	27.0	0.376	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
227.2	10.0	27.0	0.372	10.1	27.0	0.373	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
FLN	10.1	27.0	0.373	10.1	27.0	0.374	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5753	--	16421	19915	16421	0	18798	252.4	10.05	2.9
Des							18798			

Trave : 314 [318 , 317] Pilastrate [12 , 34]

Sez. R: By= 50.0 cm Bz=30.0 cm L=375.1 cm Ln=375.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5915	3565	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	3.2
37.5	3971	3630	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	4.7
CAMP	--	3456	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-I-3	5.4
337.5	4843	2605	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	3.9
FLN	7085	2242	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	2.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.379	10.1	27.0	0.376	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
37.5	10.2	27.0	0.376	10.1	27.0	0.376	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
CAMP	--	--	--	10.1	27.0	0.376	18798	18798	(3+4)-II-2	(5+6)-I-3	--	Parz.
337.5	10.2	27.0	0.378	10.1	27.0	0.374	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
FLN	10.3	27.0	0.381	10.1	27.0	0.374	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7149	--	16421	19915	16421	0	18798	375.0	10.05	2.3
Des							18798			

Trave : 315 [323 , 329] Pilastrate [29 , 8]

Sez. R: By= 50.0 cm Bz=30.0 cm L=288.5 cm Ln=288.5 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	8997	7524	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	2.1
28.8	7322	6387	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	2.6
CAMP	5683	5214	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	3.3
259.6	4009	4779	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.9

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
FLN	5470	6129	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.384	10.3	27.0	0.382	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
28.8	10.3	27.0	0.381	10.3	27.0	0.380	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
CAMP	10.2	27.0	0.379	10.2	27.0	0.378	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
259.6	10.2	27.0	0.376	10.2	27.0	0.377	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
FLN	10.2	27.0	0.378	10.2	27.0	0.379	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (5+6)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7489	--	16421	19915	16421	0	18798	288.5	10.05	2.2
Des							18798			

Trave : 315 [317 , 323] Pilastrate [34 , 29]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 475.0 \text{ cm}$ $L_n = 475.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	7330	6060	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	2.6
47.5	5622	5092	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	3.3
CAMP	4052	1777	--	--	14.07	14.07	18798	18798	(5+6)-II-2	(3+4)-I-3	4.6
427.5	5697	5002	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.3
FLN	7426	5949	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	2.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.381	10.2	27.0	0.379	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
47.5	10.2	27.0	0.379	10.2	27.0	0.378	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
CAMP	10.2	27.0	0.376	10.1	27.0	0.373	18798	18798	(5+6)-II-2	(3+4)-I-3	Parz.	Parz.
427.5	10.2	27.0	0.379	10.2	27.0	0.378	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
FLN	10.3	27.0	0.381	10.2	27.0	0.379	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb = (3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4668	--	16421	19915	16421	0	18798	475.0	10.05	3.5
Des							18798			

Trave : 316 [328 , 322] Pilastrate [5 , 28]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 472.3 \text{ cm}$ $L_n = 481.1 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5295	4407	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	3.6
48.1	3860	3698	--	--	14.07	14.07	18798	18798	(3+4)-II-2	(5+6)-II-1	4.9
CAMP	3775	3672	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	5.0
433.0	5197	4394	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	3.6
FLN	6705	5029	--	--	14.07	14.07	18798	18798	(5+6)-II-1	(3+4)-II-2	2.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.378	10.2	27.0	0.377	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
48.1	10.2	27.0	0.376	10.1	27.0	0.376	18798	18798	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.2	27.0	0.376	10.1	27.0	0.376	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
433.0	10.2	27.0	0.378	10.2	27.0	0.377	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.380	10.2	27.0	0.378	18798	18798	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	3967	--	16421	19915	16421	0	18798	481.1	10.05	4.1
Des							18798			

Trave : 317 [327 , 0] Pilastrate [6 , -]

Sez. R: By= 60.0 cm Bz=30.0 cm L=458.5 cm Ln=449.2 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	8995	1020	--	--	18.10	18.10	24144	24144	(3+4)-II-2	(5+6)-II-1	2.7
44.9	5764	2569	--	--	18.10	18.10	24144	24144	(3+4)-II-2	(5+6)-II-1	4.2
CAMP	--	6548	--	--	18.10	18.10	24144	24144	(3+4)-I-3	2	3.7
404.3	968	4158	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	5.8
FLN	3360	3447	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	7.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.5	27.0	0.387	10.2	27.0	0.378	24144	24144	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
44.9	10.4	27.0	0.383	10.3	27.0	0.380	24144	24144	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	--	--	--	10.4	27.0	0.384	24144	24144	(3+4)-I-3	2	--	Parz.
404.3	10.2	27.0	0.378	10.3	27.0	0.382	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	10.3	27.0	0.381	10.3	27.0	0.381	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	10367	--	19705	19915	19705	0	24144	449.2	10.05	1.9
Des							24144			

Trave : 317 [0 , 321] Pilastrate [- , 27]

Sez. R: By= 60.0 cm Bz=30.0 cm L=140.0 cm Ln=137.9 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3318	4025	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	6.0
13.8	4161	3629	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	5.8
CAMP	10304	3224	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	2.3
124.1	11216	156	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	2.2
FLN	12137	--	--	--	18.10	18.10	24144	24144	(5+6)-II-1	(3+4)-II-2	2.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.381	10.3	27.0	0.382	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
13.8	10.3	27.0	0.382	10.3	27.0	0.381	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
CAMP	10.5	27.0	0.389	10.3	27.0	0.381	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
124.1	10.5	27.0	0.390	10.2	27.0	0.377	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	10.6	27.0	0.391	--	--	--	24144	24144	(5+6)-II-1	(3+4)-II-2	Parz.	--

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8613	--	19705	19915	19705	0	24144	137.9	10.05	2.3
Des							24144			

Trave : 318 [319 , 0] Pilastrate [16 , -]

Sez. R: $B_y = 60.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 253.0 \text{ cm}$ $L_n = 238.9 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5920	2268	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	4.1
23.9	4659	2679	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	5.2
CAMP	3498	3329	--	--	18.10	18.10	24144	24144	(3+4)-I-3	(5+6)-I-1	6.9
215.0	--	3323	--	--	18.10	18.10	24144	24144	(3+4)-II-1	2	7.3
FLN	--	3146	--	--	18.10	18.10	24144	24144	(3+4)-II-1	2	7.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.384	10.2	27.0	0.380	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
23.9	10.3	27.0	0.382	10.3	27.0	0.380	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.381	10.3	27.0	0.381	24144	24144	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
215.0	--	--	--	10.3	27.0	0.381	24144	24144	(3+4)-II-1	2	--	Parz.
FLN	--	--	--	10.3	27.0	0.381	24144	24144	(3+4)-II-1	2	--	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6242	--	19705	19915	19705	0	24144	238.9	10.05	3.2
Des							24144			

Trave : 318 [0 , 320] Pilastrate [- , 26]

Sez. R: $B_y = 60.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 257.2 \text{ cm}$ $L_n = 249.6 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	--	3461	--	--	18.10	18.10	24144	24144	(3+4)-II-1	2	7.0
25.0	--	2869	--	--	18.10	18.10	24144	24144	(3+4)-I-1	2	8.4
CAMP	5404	2715	--	--	18.10	18.10	24144	24144	(5+6)-I-1	(5+6)-I-3	4.5
224.6	6478	2522	--	--	18.10	18.10	24144	24144	(5+6)-I-1	(3+4)-I-3	3.7
FLN	7580	2405	--	--	18.10	18.10	24144	24144	(5+6)-I-1	(3+4)-I-3	3.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	--	--	--	10.3	27.0	0.381	24144	24144	(3+4)-II-1	2	--	Parz.
25.0	--	--	--	10.3	27.0	0.380	24144	24144	(3+4)-I-1	2	--	Parz.
CAMP	10.3	27.0	0.383	10.3	27.0	0.380	24144	24144	(5+6)-I-1	(5+6)-I-3	Parz.	Parz.
224.6	10.4	27.0	0.384	10.3	27.0	0.380	24144	24144	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
FLN	10.4	27.0	0.386	10.3	27.0	0.380	24144	24144	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5130	--	19705	19915	19705	0	24144	249.6	10.05	3.8
Des							24144			

Trave : 319 [315 , 0] Pilastrate [17 , -]

Sez. R: By= 50.0 cm Bz=30.0 cm L=253.0 cm Ln=252.4 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5532	3470	--	--	18.10	18.10	24093	24093	(3+4)-I-3	(5+6)-I-1	4.4
25.2	4423	3428	--	--	18.10	18.10	24093	24093	(3+4)-I-3	(5+6)-I-1	5.4
CAMP	3395	3306	--	--	18.10	18.10	24093	24093	(3+4)-I-3	(5+6)-I-1	7.1
227.2	--	1574	--	--	18.10	18.10	24093	24093	(3+4)-I-1	(5+6)-I-3	15
FLN	618	1942	--	--	18.10	18.10	24093	24093	(3+4)-I-1	(5+6)-I-3	12

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.8	27.0	0.400	10.7	27.0	0.398	24093	24093	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
25.2	10.8	27.0	0.399	10.7	27.0	0.397	24093	24093	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.7	27.0	0.397	10.7	27.0	0.397	24093	24093	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
227.2	--	--	--	10.7	27.0	0.395	24093	24093	(3+4)-I-1	(5+6)-I-3	--	Parz.
FLN	10.6	27.0	0.394	10.7	27.0	0.396	24093	24093	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5312	--	16421	19915	16421	0	24093	252.4	10.05	3.1
Des							24093			

Trave : 319 [0 , 316] Pilastrate [- , 31]

Sez. R: By= 50.0 cm Bz=30.0 cm L=142.1 cm Ln=142.1 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	577	2412	--	--	18.10	18.10	24093	24093	(5+6)-I-1	(3+4)-I-3	10.0
14.2	1089	2545	--	--	18.10	18.10	24093	24093	(5+6)-I-1	(3+4)-I-3	9.5
CAMP	4892	3269	--	--	18.10	18.10	24093	24093	(5+6)-I-1	(3+4)-I-3	4.9
127.9	5466	3342	--	--	18.10	18.10	24093	24093	(5+6)-I-1	(3+4)-I-3	4.4
FLN	6047	3408	--	--	18.10	18.10	24093	24093	(5+6)-I-1	(3+4)-I-3	4.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.6	27.0	0.394	10.7	27.0	0.396	24093	24093	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
14.2	10.7	27.0	0.395	10.7	27.0	0.396	24093	24093	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
CAMP	10.8	27.0	0.399	10.7	27.0	0.397	24093	24093	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
127.9	10.8	27.0	0.400	10.7	27.0	0.397	24093	24093	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
FLN	10.8	27.0	0.401	10.7	27.0	0.397	24093	24093	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	4877	--	16421	19915	16421	0	24093	142.1	10.05	3.4
Des							24093			

Trave : 320 [311 , 0] Pilastrate [18 , -]

Sez. R: By= 50.0 cm Bz=30.0 cm L=253.0 cm Ln=252.4 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6180	4089	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	3.0
25.2	4994	3960	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	3.8
CAMP	3887	3751	--	--	14.07	14.07	18798	18798	(3+4)-I-3	(5+6)-I-1	4.8
227.2	--	1659	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	11
FLN	820	2113	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	8.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.380	10.2	27.0	0.376	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
25.2	10.2	27.0	0.378	10.2	27.0	0.376	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.2	27.0	0.376	10.2	27.0	0.376	18798	18798	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
227.2	--	--	--	10.1	27.0	0.373	18798	18798	(3+4)-I-1	(5+6)-I-3	--	Parz.
FLN	10.0	27.0	0.372	10.1	27.0	0.374	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio:cot(θ)=2.500

Comb =(3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5727	--	16421	19915	16421	0	18798	252.4	10.05	2.9
Des							18798			

Trave : 320 [0 , 312] Pilastrate [- , 33]

Sez. R: By= 50.0 cm Bz=30.0 cm L=142.1 cm Ln=142.1 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	817	2476	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	7.6
14.2	1345	2641	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	7.1
CAMP	5268	3589	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	3.6
127.9	5859	3694	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	3.2
FLN	6458	3792	--	--	14.07	14.07	18798	18798	(5+6)-I-1	(3+4)-I-3	2.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.0	27.0	0.372	10.1	27.0	0.374	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
14.2	10.1	27.0	0.373	10.1	27.0	0.374	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
CAMP	10.2	27.0	0.378	10.1	27.0	0.376	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
127.9	10.2	27.0	0.379	10.1	27.0	0.376	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
FLN	10.3	27.0	0.380	10.2	27.0	0.376	18798	18798	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.

Verifica a taglio:cot(θ)=2.500

Comb =(5+6)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5058	--	16421	19915	16421	0	18798	142.1	10.05	3.2
Des							18798			

Trave : 321 [322 , 323] Pilastrate [28 , 29]

Sez. R: By= 50.0 cm Bz=30.0 cm L=480.0 cm Ln=465.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5:: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6705	2914	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	2.8
46.5	4597	3126	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	4.1
CAMP	2773	3054	--	--	14.07	14.07	18798	18798	(5+6)-I-3	(3+4)-I-1	6.2
418.5	4742	2701	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	4.0
FLN	6805	2533	--	--	14.07	14.07	18798	18798	(3+4)-I-1	(5+6)-I-3	2.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.380	10.1	27.0	0.375	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
46.5	10.2	27.0	0.377	10.1	27.0	0.375	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
CAMP	10.1	27.0	0.375	10.1	27.0	0.375	18798	18798	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
418.5	10.2	27.0	0.377	10.1	27.0	0.374	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.3	27.0	0.380	10.1	27.0	0.374	18798	18798	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =(5+6)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5521	--	16421	19915	16421	0	18798	465.0	10.05	3.0
Des							18798			

Trave : 322 [0 , 0] Pilastrate [- , -]

Sez. R: By= 20.0 cm Bz=30.0 cm L=253.0 cm Ln=253.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5:: **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2078	1570	--	--	6.03	6.03	8048	8048	(3+4)-I-3	(5+6)-I-1	3.9
25.3	1827	1492	--	--	6.03	6.03	8048	8048	(3+4)-I-3	(5+6)-I-1	4.4
CAMP	1585	1405	--	--	6.03	6.03	8048	8048	(3+4)-I-3	(5+6)-I-1	5.1
227.7	165	529	--	--	6.03	6.03	8048	8048	(3+4)-I-3	(5+6)-I-1	15
FLN	32	397	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	20

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.384	10.3	27.0	0.382	8048	8048	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
25.3	10.3	27.0	0.383	10.3	27.0	0.382	8048	8048	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.382	10.3	27.0	0.382	8048	8048	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
227.7	10.2	27.0	0.378	10.2	27.0	0.379	8048	8048	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
FLN	10.2	27.0	0.377	10.2	27.0	0.378	8048	8048	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =(3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1230	--	6568	9957	6568	0	8048	253.0	5.03	5.3
Des							8048			

Trave : 322 [0 , 0] Pilastrate [- , -]

Sez. R: By= 20.0 cm Bz=30.0 cm L=592.2 cm Ln=592.2 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$
::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	208	264	--	--	6.03	6.03	8048	8048	(3+4)-I-3	(5+6)-I-1	30
59.2	--	326	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	25
CAMP	1220	941	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	6.6
533.0	1642	793	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	4.9
FLN	2115	640	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	3.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.378	10.2	27.0	0.378	8048	8048	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
59.2	--	--	--	10.2	27.0	0.378	8048	8048	(3+4)-II-2	(5+6)-II-1	--	Parz.
CAMP	10.3	27.0	0.381	10.3	27.0	0.380	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
533.0	10.3	27.0	0.383	10.3	27.0	0.380	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.4	27.0	0.384	10.2	27.0	0.379	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	935	--	6568	9957	6568	0	8048	592.2	5.03	7.0
Des							8048			

Trave : 323 [0 , 0] Pilastrate [- , -]

Sez. R: $B_y = 20.0$ cm $B_z = 30.0$ cm $L = 441.4$ cm $L_n = 431.4$ cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$
::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2296	1680	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	3.5
43.1	1799	1449	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	4.5
CAMP	1331	1189	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	6.0
388.3	1414	1164	--	--	6.03	6.03	8048	8048	(5+6)-II-1	(3+4)-II-2	5.7
FLN	1898	1409	--	--	6.03	6.03	8048	8048	(5+6)-II-1	(3+4)-II-2	4.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.385	10.3	27.0	0.383	8048	8048	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
43.1	10.3	27.0	0.383	10.3	27.0	0.382	8048	8048	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.3	27.0	0.381	10.3	27.0	0.381	8048	8048	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
388.3	10.3	27.0	0.382	10.3	27.0	0.381	8048	8048	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	10.4	27.0	0.383	10.3	27.0	0.382	8048	8048	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1464	--	6568	9957	6568	0	8048	431.4	5.03	4.5
Des							8048			

Trave : 323 [0 , 0] Pilastrate [- , -]

Sez. R: $B_y = 20.0$ cm $B_z = 30.0$ cm $L = 160.0$ cm $L_n = 160.0$ cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$
::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
ILN	1461	--	--	--	6.03	6.03	8048	8048	(5+6)-II-2	(3+4)-II-1	5.5
16.0	1346	--	--	--	6.03	6.03	8048	8048	(5+6)-II-2	(3+4)-II-1	6.0
CAMP	1235	--	--	--	6.03	6.03	8048	8048	(5+6)-II-2	(3+4)-II-1	6.5
144.0	578	181	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	14
FLN	503	216	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	16

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.382	--	--	--	8048	8048	(5+6)-II-2	(3+4)-II-1	Parz.	--
16.0	10.3	27.0	0.382	--	--	--	8048	8048	(5+6)-II-2	(3+4)-II-1	Parz.	--
CAMP	10.3	27.0	0.381	--	--	--	8048	8048	(5+6)-II-2	(3+4)-II-1	Parz.	--
144.0	10.2	27.0	0.379	10.2	27.0	0.378	8048	8048	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
FLN	10.2	27.0	0.379	10.2	27.0	0.378	8048	8048	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1065	--	6568	9957	6568	0	8048	160.0	5.03	6.2
Des							8048			

Trave : 324 [0 , 0] Pilastrate [- , -]

Sez. R: By= 20.0 cm Bz=30.0 cm L=597.8 cm Ln=597.8 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2187	713	--	--	6.03	6.03	8048	8048	(3+4)-I-3	(5+6)-I-1	3.7
59.8	1695	853	--	--	6.03	6.03	8048	8048	(3+4)-I-3	(5+6)-I-1	4.7
CAMP	1258	971	--	--	6.03	6.03	8048	8048	(3+4)-I-3	(5+6)-I-1	6.4
538.0	--	343	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	23
FLN	318	326	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	25

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.384	10.2	27.0	0.379	8048	8048	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
59.8	10.3	27.0	0.383	10.3	27.0	0.380	8048	8048	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.381	10.3	27.0	0.380	8048	8048	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
538.0	--	--	--	10.2	27.0	0.378	8048	8048	(3+4)-II-2	(5+6)-II-1	--	Parz.
FLN	10.2	27.0	0.378	10.2	27.0	0.378	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	965	--	6568	9957	6568	0	8048	597.8	5.03	6.8
Des							8048			

Trave : 324 [0 , 0] Pilastrate [- , -]

Sez. R: By= 20.0 cm Bz=30.0 cm L=247.6 cm Ln=247.6 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cmq], $f_{ym}=4500$ [kg/cmq], $FC=1.20$ $q_d=2$, $q_f=1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	99	435	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	18
24.8	232	571	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	14
CAMP	1478	1308	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	5.4

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
222.8	1694	1378	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	4.8
FLN	1920	1438	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	4.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.378	10.2	27.0	0.379	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
24.8	10.2	27.0	0.378	10.2	27.0	0.379	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
CAMP	10.3	27.0	0.382	10.3	27.0	0.381	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
222.8	10.3	27.0	0.383	10.3	27.0	0.382	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.4	27.0	0.383	10.3	27.0	0.382	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1124	--	6568	9957	6568	0	8048	247.6	5.03	5.8
Des							8048			

Trave : 325 [0, 0] Pilastrate [- , -]

Sez. R: $B_y = 20.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 441.8 \text{ cm}$ $L_n = 431.8 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2445	1761	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	3.3
43.2	1921	1515	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	4.2
CAMP	1426	1241	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	5.6
388.6	1460	1259	--	--	6.03	6.03	8048	8048	(5+6)-II-1	(3+4)-II-2	5.5
FLN	1957	1531	--	--	6.03	6.03	8048	8048	(5+6)-II-1	(3+4)-II-2	4.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.4	27.0	0.385	10.3	27.0	0.383	8048	8048	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
43.2	10.4	27.0	0.383	10.3	27.0	0.382	8048	8048	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	10.3	27.0	0.382	10.3	27.0	0.381	8048	8048	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
388.6	10.3	27.0	0.382	10.3	27.0	0.381	8048	8048	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	10.4	27.0	0.384	10.3	27.0	0.382	8048	8048	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1542	--	6568	9957	6568	0	8048	431.8	5.03	4.3
Des							8048			

Trave : 325 [0, 0] Pilastrate [- , -]

Sez. R: $B_y = 20.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 159.9 \text{ cm}$ $L_n = 159.9 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1618	--	--	--	6.03	6.03	8048	8048	(5+6)-II-2	(3+4)-II-1	5.0
16.0	1492	--	--	--	6.03	6.03	8048	8048	(5+6)-II-2	(3+4)-II-1	5.4
CAMP	1371	190	--	--	6.03	6.03	8048	8048	(5+6)-II-2	(5+6)-II-1	5.9
143.9	650	226	--	--	6.03	6.03	8048	8048	(3+4)-II-2	(5+6)-II-1	12
FLN	597	287	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	13

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.382	--	--	--	8048	8048	(5+6)-II-2	(3+4)-II-1	Parz.	--
16.0	10.3	27.0	0.382	--	--	--	8048	8048	(5+6)-II-2	(3+4)-II-1	Parz.	--
CAMP	10.3	27.0	0.382	10.2	27.0	0.378	8048	8048	(5+6)-II-2	(5+6)-II-1	Parz.	Parz.
143.9	10.2	27.0	0.379	10.2	27.0	0.378	8048	8048	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
FLN	10.2	27.0	0.379	10.2	27.0	0.378	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	961	--	6568	9957	6568	0	8048	159.9	5.03	6.8
Des							8048			

Trave : 326 [0 , 0] Pilastrate [- , -]

Sez. R: $B_y = 20.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 253.0 \text{ cm}$ $L_n = 238.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1277	872	--	--	6.03	6.03	8048	8048	(3+4)-I-3	(5+6)-I-1	6.3
23.8	1108	851	--	--	6.03	6.03	8048	8048	(3+4)-I-3	(5+6)-I-1	7.3
CAMP	948	821	--	--	6.03	6.03	8048	8048	(3+4)-I-3	(5+6)-I-1	8.5
214.2	70	382	--	--	6.03	6.03	8048	8048	(3+4)-I-3	(5+6)-I-1	21
FLN	38	345	--	--	6.03	6.03	8048	8048	(3+4)-II-1	(5+6)-II-2	23

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.381	10.3	27.0	0.380	8048	8048	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
23.8	10.3	27.0	0.381	10.3	27.0	0.380	8048	8048	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	10.3	27.0	0.380	10.3	27.0	0.380	8048	8048	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
214.2	10.2	27.0	0.377	10.2	27.0	0.378	8048	8048	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
FLN	10.2	27.0	0.377	10.2	27.0	0.378	8048	8048	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	860	--	6568	9957	6568	0	8048	238.0	5.03	7.6
Des							8048			

Trave : 326 [0 , 0] Pilastrate [- , -]

Sez. R: $B_y = 20.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 598.5 \text{ cm}$ $L_n = 587.9 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	152	87	--	--	6.03	6.03	8048	8048	(5+6)-II-1	(3+4)-II-2	53
58.8	--	257	--	--	6.03	6.03	8048	8048	(3+4)-II-1	(5+6)-II-2	31
CAMP	648	665	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	12
529.1	969	353	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	8.3
FLN	1341	146	--	--	6.03	6.03	8048	8048	(3+4)-I-1	(5+6)-I-3	6.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.378	10.2	27.0	0.377	8048	8048	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
58.8	--	--	--	10.2	27.0	0.378	8048	8048	(3+4)-II-1	(5+6)-II-2	--	Parz.
CAMP	10.2	27.0	0.379	10.2	27.0	0.379	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
529.1	10.3	27.0	0.380	10.2	27.0	0.378	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	10.3	27.0	0.382	10.2	27.0	0.378	8048	8048	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	725	--	6568	9957	6568	0	8048	587.9	5.03	9.1
Des							8048			

Trave : 327 [0 , 0] Pilastrate [- , -]

Sez. R: $B_y = 20.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 147.6 \text{ cm}$ $L_n = 142.5 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	628	201	--	--	6.03	6.03	8048	8048	(3+4)-II-1	(5+6)-II-2	13
14.2	712	175	--	--	6.03	6.03	8048	8048	(5+6)-II-1	(3+4)-II-2	11
CAMP	1399	148	--	--	6.03	6.03	8048	8048	(5+6)-II-1	(3+4)-II-2	5.8
128.2	1510	--	--	--	6.03	6.03	8048	8048	(5+6)-II-1	(3+4)-II-2	5.3
FLN	1624	--	--	--	6.03	6.03	8048	8048	(5+6)-II-1	(3+4)-II-2	5.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.2	27.0	0.379	10.2	27.0	0.378	8048	8048	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
14.2	10.2	27.0	0.379	10.2	27.0	0.378	8048	8048	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
CAMP	10.3	27.0	0.382	10.2	27.0	0.378	8048	8048	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
128.2	10.3	27.0	0.382	--	--	--	8048	8048	(5+6)-II-1	(3+4)-II-2	Parz.	--
FLN	10.3	27.0	0.382	--	--	--	8048	8048	(5+6)-II-1	(3+4)-II-2	Parz.	--

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	929	--	6568	9957	6568	0	8048	142.5	5.03	7.1
Des							8048			

Trave : 327 [0 , 0] Pilastrate [- , -]

Sez. R: $B_y = 20.0 \text{ cm}$ $B_z = 30.0 \text{ cm}$ $L = 463.8 \text{ cm}$ $L_n = 463.8 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	1811	1302	--	--	6.03	6.03	8048	8048	(5+6)-II-2	(3+4)-II-1	4.4
46.4	1336	1096	--	--	6.03	6.03	8048	8048	(5+6)-II-2	(3+4)-II-1	6.0
CAMP	1249	1080	--	--	6.03	6.03	8048	8048	(3+4)-II-1	(5+6)-II-2	6.4
417.4	1713	1295	--	--	6.03	6.03	8048	8048	(3+4)-II-1	(5+6)-II-2	4.7
FLN	2210	1479	--	--	6.03	6.03	8048	8048	(3+4)-II-1	(5+6)-II-2	3.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	10.3	27.0	0.383	10.3	27.0	0.381	8048	8048	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
46.4	10.3	27.0	0.382	10.3	27.0	0.381	8048	8048	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
CAMP	10.3	27.0	0.381	10.3	27.0	0.381	8048	8048	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
417.4	10.3	27.0	0.383	10.3	27.0	0.381	8048	8048	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
FLN	10.4	27.0	0.384	10.3	27.0	0.382	8048	8048	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	1350	--	6568	9957	6568	0	8048	463.8	5.03	4.9
Des							8048			

Trave : 401 [417 , 423] Pilastrate [34 , 29]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 45.0 \text{ cm}$ $L = 475.0 \text{ cm}$ $L_n = 460.4 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6972	1250	--	--	20.11	20.11	43154	43154	(3+4)-II-1	(5+6)-II-2	6.2
46.0	3803	1114	--	--	20.11	20.11	43154	43154	(3+4)-II-1	(5+6)-II-2	11
CAMP	3774	5960	--	--	20.11	20.11	43154	43154	(3+4)-II-2	(5+6)-II-1	7.2
414.4	5810	7170	--	--	20.11	20.11	43154	43154	(3+4)-II-2	(5+6)-II-1	6.0
FLN	7967	8261	--	--	20.11	20.11	43154	43154	(3+4)-II-2	(5+6)-II-1	5.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	15.0	42.0	0.357	14.9	42.0	0.354	43154	43154	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
46.0	14.9	42.0	0.355	14.9	42.0	0.354	43154	43154	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
CAMP	14.9	42.0	0.355	15.0	42.0	0.356	43154	43154	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
414.4	15.0	42.0	0.356	15.0	42.0	0.357	43154	43154	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
FLN	15.0	42.0	0.357	15.0	42.0	0.358	43154	43154	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8222	--	25544	30979	25544	0	43154	460.4	10.05	3.1
Des							43154			

Trave : 401 [413 , 417] Pilastrate [32 , 34]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 45.0 \text{ cm}$ $L = 310.0 \text{ cm}$ $L_n = 310.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

::Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5328	1845	--	--	20.11	20.11	43154	43154	(5+6)-II-1	(3+4)-II-2	8.1
31.0	3632	1819	--	--	20.11	20.11	43154	43154	(5+6)-II-1	(3+4)-II-2	12
CAMP	1994	1775	--	--	20.11	20.11	43154	43154	(3+4)-II-1	(5+6)-II-2	22
279.0	3469	458	--	--	20.11	20.11	43154	43154	(3+4)-II-2	(5+6)-II-1	12
FLN	5345	300	--	--	20.11	20.11	43154	43154	(3+4)-II-2	(5+6)-II-1	8.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	15.0	42.0	0.356	14.9	42.0	0.354	43154	43154	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
31.0	14.9	42.0	0.355	14.9	42.0	0.354	43154	43154	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
CAMP	14.9	42.0	0.354	14.9	42.0	0.354	43154	43154	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
279.0	14.9	42.0	0.355	14.8	42.0	0.353	43154	43154	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
FLN	15.0	42.0	0.356	14.8	42.0	0.353	43154	43154	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7068	--	25544	30979	25544	0	43154	310.0	10.05	3.6
Des							43154			

Trave : 402 [421 , 420] Pilastrate [27 , 26]

Sez. R: By= 50.0 cm Bz=45.0 cm L=345.0 cm Ln=345.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	4472	633	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-I-3	9.6
34.5	2677	794	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-I-3	16
CAMP	--	3690	--	--	20.11	20.11	43154	43154	(3+4)-II-2	(3+4)-I-1	12
310.5	1262	4072	--	--	20.11	20.11	43154	43154	(5+6)-I-3	(3+4)-I-1	11
FLN	2210	4388	--	--	20.11	20.11	43154	43154	(5+6)-I-3	(3+4)-I-1	9.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.9	42.0	0.356	14.9	42.0	0.354	43154	43154	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
34.5	14.9	42.0	0.355	14.9	42.0	0.354	43154	43154	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
CAMP	--	--	--	14.9	42.0	0.355	43154	43154	(3+4)-II-2	(3+4)-I-1	--	Parz.
310.5	14.9	42.0	0.354	14.9	42.0	0.355	43154	43154	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.
FLN	14.9	42.0	0.354	14.9	42.0	0.356	43154	43154	(5+6)-I-3	(3+4)-I-1	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6089	--	25544	30979	25544	0	43154	345.0	10.05	4.2
Des							43154			

Trave : 402 [422 , 421] Pilastrate [28 , 27]

Sez. R: By= 50.0 cm Bz=45.0 cm L=310.0 cm Ln=325.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm}=200$ [kg/cm²], $f_{ym}=4500$ [kg/cm²], FC=1.20 qd=2, qf=1.5

:: Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	3837	--	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-I-3	11
32.5	2605	--	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-I-3	17
CAMP	1434	690	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-II-1	30
292.5	2044	119	--	--	20.11	20.11	43154	43154	(3+4)-I-3	(5+6)-I-1	21
FLN	3319	--	--	--	20.11	20.11	43154	43154	(3+4)-I-3	(5+6)-I-1	13

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.9	42.0	0.355	--	--	--	43154	43154	(3+4)-I-1	(5+6)-I-3	Parz.	--
32.5	14.9	42.0	0.355	--	--	--	43154	43154	(3+4)-I-1	(5+6)-I-3	Parz.	--
CAMP	14.9	42.0	0.354	14.9	42.0	0.354	43154	43154	(3+4)-I-1	(5+6)-II-1	Parz.	Parz.
292.5	14.9	42.0	0.354	14.8	42.0	0.353	43154	43154	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
FLN	14.9	42.0	0.355	--	--	--	43154	43154	(3+4)-I-3	(5+6)-I-1	Parz.	--

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
Sin	4477	--	25544	30979	25544	0	43154	325.0	10.05	5.7
Des							43154			

Trave : 402 [422 , 423] Pilastrate [28 , 29]

Sez. R: By= 50.0 cm Bz=45.0 cm L=480.0 cm Ln=465.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	4840	--	--	--	20.11	20.11	43154	43154	(3+4)-I-3	(5+6)-I-1	8.9
46.5	2415	281	--	--	20.11	20.11	43154	43154	(3+4)-I-3	(5+6)-I-1	18
CAMP	--	3365	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-I-3	13
418.5	1490	3299	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-I-3	13
FLN	2642	3113	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-I-3	14

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.9	42.0	0.356	--	--	--	43154	43154	(3+4)-I-3	(5+6)-I-1	Parz.	--
46.5	14.9	42.0	0.355	14.8	42.0	0.353	43154	43154	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	--	--	--	14.9	42.0	0.355	43154	43154	(3+4)-I-1	(5+6)-I-3	--	Parz.
418.5	14.9	42.0	0.354	14.9	42.0	0.355	43154	43154	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	14.9	42.0	0.355	14.9	42.0	0.355	43154	43154	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio:cot(θ)=2.500

Comb =(3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5958	--	25544	30979	25544	0	43154	465.0	10.05	4.3
Des							43154			

Trave : 403 [420 , 416] Pilastrate [26 , 31]

Sez. R: By= 50.0 cm Bz=45.0 cm L=488.7 cm Ln=469.7 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cmq],fym=4500 [kg/cmq], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	8171	7329	--	--	20.11	20.11	43154	43154	(5+6)-II-2	(3+4)-II-1	5.3
47.0	5596	6779	--	--	20.11	20.11	43154	43154	(5+6)-II-2	(3+4)-II-1	6.4
CAMP	3227	6032	--	--	20.11	20.11	43154	43154	(5+6)-II-2	(3+4)-II-1	7.2
422.7	3466	1161	--	--	20.11	20.11	43154	43154	(3+4)-II-1	(5+6)-II-2	12
FLN	6934	776	--	--	20.11	20.11	43154	43154	(3+4)-II-1	(5+6)-II-2	6.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	15.0	42.0	0.358	15.0	42.0	0.357	43154	43154	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
47.0	15.0	42.0	0.356	15.0	42.0	0.357	43154	43154	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
CAMP	14.9	42.0	0.355	15.0	42.0	0.356	43154	43154	(5+6)-II-2	(3+4)-II-1	Parz.	Parz.
422.7	14.9	42.0	0.355	14.9	42.0	0.354	43154	43154	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	15.0	42.0	0.357	14.9	42.0	0.354	43154	43154	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio:cot(θ)=2.500

Comb =(3+4)-II-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8627	--	25544	30979	25544	0	43154	469.7	10.05	3.0
Des							43154			

Trave : 403 [416 , 412] Pilastrate [31 , 33]

Sez. R: By= 50.0 cm Bz=45.0 cm L=310.0 cm Ln=310.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5269	889	--	--	20.11	20.11	43154	43154	(3+4)-II-2	(5+6)-II-1	8.2
31.0	3433	982	--	--	20.11	20.11	43154	43154	(3+4)-II-2	(5+6)-II-1	13
CAMP	1820	1292	--	--	20.11	20.11	43154	43154	(3+4)-II-1	(5+6)-I-1	24
279.0	3550	1375	--	--	20.11	20.11	43154	43154	(3+4)-II-1	(5+6)-II-2	12
FLN	5339	1322	--	--	20.11	20.11	43154	43154	(3+4)-II-1	(5+6)-II-2	8.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	15.0	42.0	0.356	14.9	42.0	0.354	43154	43154	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
31.0	14.9	42.0	0.355	14.9	42.0	0.354	43154	43154	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	14.9	42.0	0.354	14.9	42.0	0.354	43154	43154	(3+4)-II-1	(5+6)-I-1	Parz.	Parz.
279.0	14.9	42.0	0.355	14.9	42.0	0.354	43154	43154	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
FLN	15.0	42.0	0.356	14.9	42.0	0.354	43154	43154	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =(3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6955	--	25544	30979	25544	0	43154	310.0	10.05	3.7
Des							43154			

Trave : 403 [412 , 406] Pilastrate [33 , 23]

Sez. R: By= 50.0 cm Bz=45.0 cm L=454.8 cm Ln=469.7 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	6205	611	--	--	20.11	20.11	43154	43154	(3+4)-II-2	(5+6)-II-1	7.0
47.0	2918	1063	--	--	20.11	20.11	43154	43154	(3+4)-II-2	(5+6)-II-1	15
CAMP	3162	5891	--	--	20.11	20.11	43154	43154	(5+6)-II-1	(3+4)-II-2	7.3
422.7	4613	5680	--	--	20.11	20.11	43154	43154	(5+6)-II-1	(3+4)-II-2	7.6
FLN	6269	5269	--	--	20.11	20.11	43154	43154	(5+6)-II-1	(3+4)-II-2	6.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	15.0	42.0	0.357	14.9	42.0	0.354	43154	43154	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
47.0	14.9	42.0	0.355	14.9	42.0	0.354	43154	43154	(3+4)-II-2	(5+6)-II-1	Parz.	Parz.
CAMP	14.9	42.0	0.355	15.0	42.0	0.356	43154	43154	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
422.7	14.9	42.0	0.356	15.0	42.0	0.356	43154	43154	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	15.0	42.0	0.357	15.0	42.0	0.356	43154	43154	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.

Verifica a taglio:cot(θ) =2.500

Comb =(3+4)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	8158	--	25544	30979	25544	0	43154	469.7	10.05	3.1
Des							43154			

Trave : 404 [406 , 407] Pilastrate [23 , 30]

Sez. R: By= 50.0 cm Bz=45.0 cm L=347.3 cm Ln=360.0 cm

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione rcm=200 [kg/cm²],fym=4500 [kg/cm²], FC=1.20 qd=2, qf=1.5

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	2930	6384	--	--	20.11	20.11	43154	43154	(3+4)-I-3	(5+6)-I-1	6.8
36.0	1976	5493	--	--	20.11	20.11	43154	43154	(3+4)-I-3	(5+6)-I-1	7.9
CAMP	--	4529	--	--	20.11	20.11	43154	43154	(3+4)-I-3	(5+6)-I-1	9.5
324.0	3519	953	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-I-3	12
FLN	5616	689	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-I-3	7.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.9	42.0	0.355	15.0	42.0	0.357	43154	43154	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
36.0	14.9	42.0	0.354	15.0	42.0	0.356	43154	43154	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	--	--	--	14.9	42.0	0.356	43154	43154	(3+4)-I-3	(5+6)-I-1	--	Parz.
324.0	14.9	42.0	0.355	14.9	42.0	0.354	43154	43154	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	15.0	42.0	0.356	14.9	42.0	0.354	43154	43154	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	6784	--	25544	30979	25544	0	43154	360.0	10.05	3.8
Des							43154			

Trave : 404 [407 , 408] Pilastrate [30 , 24]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 45.0 \text{ cm}$ $L = 310.0 \text{ cm}$ $L_n = 310.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	4288	502	--	--	20.11	20.11	43154	43154	(3+4)-I-3	(5+6)-I-1	10
31.0	2826	817	--	--	20.11	20.11	43154	43154	(3+4)-I-3	(5+6)-I-1	15
CAMP	1470	1412	--	--	20.11	20.11	43154	43154	(3+4)-II-1	(5+6)-II-2	29
279.0	2615	107	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-I-3	17
FLN	4147	--	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-I-3	10

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	14.9	42.0	0.355	14.8	42.0	0.354	43154	43154	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
31.0	14.9	42.0	0.355	14.9	42.0	0.354	43154	43154	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	14.9	42.0	0.354	14.9	42.0	0.354	43154	43154	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.
279.0	14.9	42.0	0.355	14.8	42.0	0.353	43154	43154	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	14.9	42.0	0.355	--	--	--	43154	43154	(3+4)-I-1	(5+6)-I-3	Parz.	--

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-1

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	5662	--	25544	30979	25544	0	43154	310.0	10.05	4.5
Des							43154			

Trave : 404 [408 , 409] Pilastrate [24 , 25]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 45.0 \text{ cm}$ $L = 347.3 \text{ cm}$ $L_n = 345.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

::Verificato

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5961	1151	--	--	20.11	20.11	43154	43154	(3+4)-I-3	(5+6)-I-1	7.2

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
34.5	3652	1298	--	--	20.11	20.11	43154	43154	(3+4)-I-3	(5+6)-I-1	12
CAMP	--	4509	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-I-3	9.6
310.5	2007	5449	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-I-3	7.9
FLN	2990	6323	--	--	20.11	20.11	43154	43154	(3+4)-I-1	(5+6)-I-3	6.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	15.0	42.0	0.356	14.9	42.0	0.354	43154	43154	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
34.5	14.9	42.0	0.355	14.9	42.0	0.354	43154	43154	(3+4)-I-3	(5+6)-I-1	Parz.	Parz.
CAMP	--	--	--	14.9	42.0	0.356	43154	43154	(3+4)-I-1	(5+6)-I-3	--	Parz.
310.5	14.9	42.0	0.354	15.0	42.0	0.356	43154	43154	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.
FLN	14.9	42.0	0.355	15.0	42.0	0.357	43154	43154	(3+4)-I-1	(5+6)-I-3	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(3+4)-I-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7844	--	25544	30979	25544	0	43154	345.0	10.05	3.3
Des							43154			

Trave : 405 [413 , 409] Pilastrate [32 , 25]

Sez. R: $B_y = 50.0 \text{ cm}$ $B_z = 45.0 \text{ cm}$ $L = 460.1 \text{ cm}$ $L_n = 474.0 \text{ cm}$

Criterio : CLS_TraviSpessore_Esist - Verifica a flessione $r_{cm} = 200 \text{ [kg/cmq]}$, $f_{ym} = 4500 \text{ [kg/cmq]}$, $FC = 1.20$ $q_d = 2$, $q_f = 1.5$

:: Verificato

X	M-	M+	$\Delta M-$	$\Delta M+$	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kg*m	kg*m	kg*m	kg*m	cmq	cmq	kg*m	kg*m			
ILN	5933	389	--	--	20.11	20.11	43154	43154	(5+6)-I-1	(3+4)-I-3	7.3
47.4	3033	1354	--	--	20.11	20.11	43154	43154	(5+6)-I-1	(3+4)-I-3	14
CAMP	2626	5532	--	--	20.11	20.11	43154	43154	(5+6)-II-1	(3+4)-II-2	7.8
426.6	4006	5130	--	--	20.11	20.11	43154	43154	(5+6)-II-1	(3+4)-II-2	8.4
FLN	5598	4528	--	--	20.11	20.11	43154	43154	(3+4)-II-1	(5+6)-II-2	7.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kg*m	kg*m				
ILN	15.0	42.0	0.356	14.8	42.0	0.353	43154	43154	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
47.4	14.9	42.0	0.355	14.9	42.0	0.354	43154	43154	(5+6)-I-1	(3+4)-I-3	Parz.	Parz.
CAMP	14.9	42.0	0.355	15.0	42.0	0.356	43154	43154	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
426.6	14.9	42.0	0.355	14.9	42.0	0.356	43154	43154	(5+6)-II-1	(3+4)-II-2	Parz.	Parz.
FLN	15.0	42.0	0.356	14.9	42.0	0.356	43154	43154	(3+4)-II-1	(5+6)-II-2	Parz.	Parz.

Verifica a taglio: $\cot(\theta) = 2.500$

Comb =(5+6)-II-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kg	kg	kg	kg	kg	kg	kg*m	cm	cmq/m	
Sin	7675	--	25544	30979	25544	0	43154	474.0	10.05	3.3
Des							43154			

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